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NUMERICAL FORECASTING OF CLEAR AIR TURBULENCE

MICHAEL JOSEPH ETTEL and WILLIAM ALLEN MORGAN

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## NUMERICAL FORECASTING OF

## CLEAR AIR TURBULENCE

by

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Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN METEOROLOGY

from the

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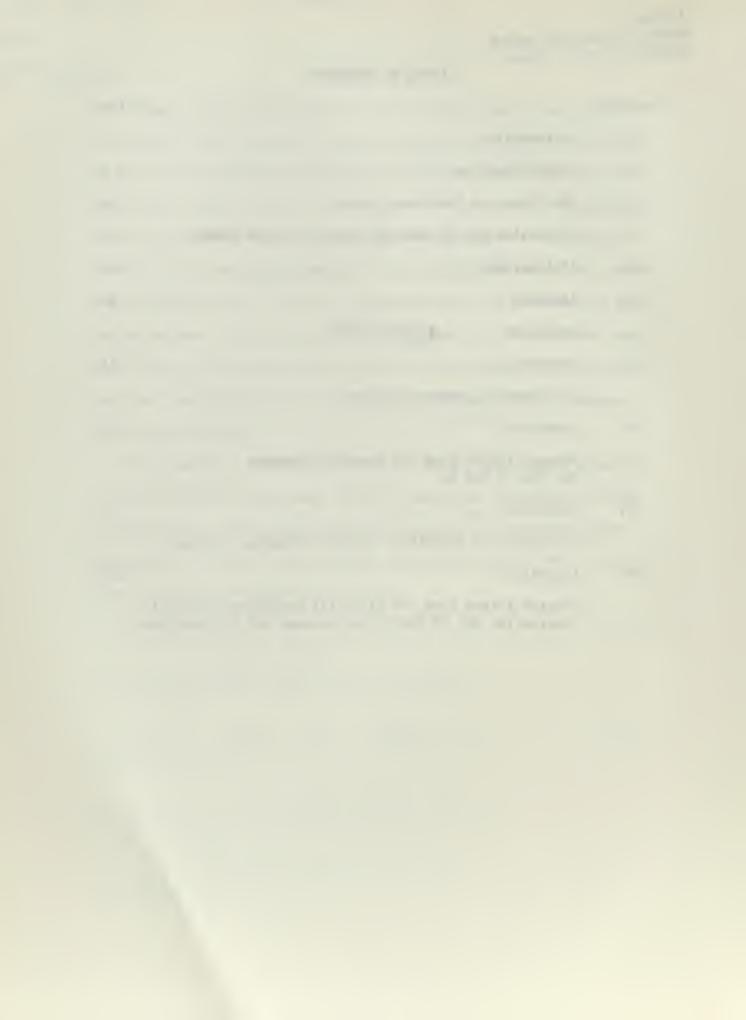
## ABSTRACT

There is much disagreement as to (a) what causes clear air turbulence (turbulence which is not in or near convective clouds and is above 15,000 feet in altitude) and (b) which meteorological parameters can be used to detect and forecast its occurrence. The approach to this problem has been to relate not one parameter to clear air turbulence but various parameters. By summing these parameters areas can be defined where there is a high probability of encountering clear air turbulence. Each parameter has been based on a statistical study which found a relationship with clear air turbulence. The parameters used were horizontal and vertical shear, curvature, kinetic energy and their derivatives.

The numerical forecasting program proposed here can be extended to the stratosphere when more reliable height and temperature fields are available. This program will have much more significance when intermediate forecast height fields, temperature fields and a grid of much smaller mesh length are available.

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#### 1. INTRODUCTION

The phenomenon of clear air turbulence (henceforth denoted as CAT) appears to consist of random three dimensional eddies that occur in certain confined regions of the atmosphere. This phenomenon was first recognized in the early 1940's as "air pockets", and has gained in importance and depth of study with the development of fast-flying swept wing and delta winged aircraft. It is of prime importance to the aviation industry because it affects the safety and comfort of passengers and crew, as well as operational costs. There have been several cases where loss of control of aircraft, structural damage, passenger and crew injuries (even deaths) have resulted from CAT.

Aircraft manufacturers and the airlines are interested in CAT in order to determine the strength of airframe design so that it can be built to withstand all degrees of turbulence. Planning of supersonic transport aircraft is considering the effects of this unexpected turbulence occurring at any flight level in the atmosphere. Therefore, it becomes an even greater operational problem in the era of future design of SST aircraft as to cost, safety and comfort. CAT is usually less intense than turbulence encountered in thunderstorms 1 . CAT may be considered at times more dangerous than "thunderstorm turbulence" as it usually occurs with no visible warning.

The various military agencies are deeply concerned with the understanding of CAT and its prediction so they may be better prepared to take it into account operationally in all areas of the world. Scientists are highly interested in CAT because it is a phenomenon of our environment that is not clearly understood. We are faced with the problem of having to rely on mesoscale data while the phenomenon is of a microscale. Because of the great differences in scales involved in the forecasting

problem, isolated patches of CAT (in either space or time) are very difficult to identify. It is the intent of this paper to develop a numerical forecasting system of CAT whereby an empirical approach has been used to accomplish this end.

## 2. DATA COLLECTION

The nature of clear air turbulence, its physics and its meteorology, are still not completely understood. More mesoscale (2km to 100km horizontal distance) and microscale (less than 2km) studies must be made concerning the causes and generation of CAT. Any improvement in forecasting skill that may be realized by this study will probably result from increased mesoscale input data into the forecast problem. The only mesoscale measurements available operationally at this time which concern the problem are rawinsonde data that give a nearly continuous measurement in the vertical of wind, pressure, temperature and humidity from the surface to above 30km in altitude, and satellite cloud pictures that delineate cloud structures down to a scale of about 3km.

The usual definition of CAT is "atmospheric turbulence which is not in or near convective clouds, including thunderstorms, and is not below 15,000 feet in altitude". (4) Thus, mechanical turbulence induced by rough terrain is excluded. It is realized that this is an extremely arbitrary definition resulting from a desire to simplify pilot reporting procedures.

Turbulence intensities are, at present, designated as light, moderate, severe and extreme. In recent years several definitions of the four categories of turbulence have been proposed. The current definitions in official use were developed by the National Advisory Committee for Aeronautics (NACA) Subcommittee on Meteorological Problems (1957). See Table 1.

There are few quantitative measurements of atmospheric turbulence at any scale. The bulk of the aircraft turbulence data available is based upon the four categories stated in Table 1, (4); and, consequently is highly subjective and qualitative in nature. Included in the factors that affect the subjective decision of the pilot when reporting turbulence are the wing loading, the aircraft's speed and attitude, the pilot's training, experience, and his psychological reactions (1).

Objective criteria for turbulence reporting must wait until more measurements are made of the conditions existing in the turbulent eddies, and until cockpit instrumentation includes a gust load or turbulence indicator.

Much time, effort and financial support have been expended in this country by the government, the aircraft industry, and private and public research facilities to investigate the problem of clear air turbulence and to find a good approach leading to a solution to this problem. This research has gone forward in three broad categories: first, research concerning the correlation of CAT with macroscale, mesoscale, and/or microscale atmospheric measurements; second, research into instrumentation for the detection of CAT sufficiently far in advance of the aircraft to allow evasive measures (6) and third, research by military and airline organizations concerning the operational aspects of CAT.

Various projects such as HICAT, ALLCAT, and TOPCAT have been undertaken to study clear air turbulence. The problems encountered were many but the results showed that it was indeed possible, with suitable instrumentation, to find, track and record CAT. The use of constant level ballons and doppler radar to detect CAT has met with some success, but again the lack of detail necessary in CAT studies leaves much to be desired.

Measurements of the microstructure, which contains the perturbations of CAT dimensions (100 to 500 meter wavelength), have been taken by specially instrumented aircraft. Until recently the aircraft itself was used as a sensor to measure atmospheric gusts from the aircraft acceleration data. The Air Force realized the danger of relying solely on the acceleration response of the U-2 aircraft as a measure of turbulence at high altitudes. A full knowledge of the aircraft's response to turbulence over a wide range of wavelengths is required for meaningful interpretation of such data. This procedure usually gives reliable results at short wavelengths up to a few hundred meters. At long wavelengths, this instrumentation becomes less sensitive. Accelerations in longer waves are usually small and can be masked by pilot induced aircraft motions.

A supersonic or hypersonic craft of some radical shape, flying four to ten times the speed of the U-2, will obviously have a somewhat different response to turbulence than the U-2. An aircraft flying at these high speeds would be affected much more by longer turbulence wavelengths and less by the shorter.

As pointed out earlier, the meteorologist has few direct measurements of turbulence intensities and must depend upon the accuracy of the intensities reported by pilots. In our study, we used the Colson monthly turbulence summaries which were obtained from the Air Force 3rd Weather Wing at Offutt AFB, Omaha, Neb. This report suited our needs most closely because the CAT reports were detailed as to location, time, altitude and intensity. In the period used in our study, December 1964 through March 1965, there were no less than 3670 CAT reports. The

reports were located over the United States and extended from about 15,000 feet to over 45,000 feet. The data were collected from military, civilian and private aircraft. They are, as mentioned before, quite subjective.

In the course of this paper three time periods or intervals will be used. It is important to establish at this point which periods were used and for what purpose.

A four month period (December 1964 through March 1965) is used for the research program during which several fields were constructed.

Patterns of fields of different meteorological parameters were sometimes similar. Then all but one of them were dropped in our further investigations. In this way only three of the original seven parameters were retained.

The three day period (10 - 12 March, 1965) was used for a verification or correlation study. During this period of time a comparison was made to find out how many times CAT actually occurred in areas where it was predicted.

Finally, 23 February 1965 was arbitrarily chosen from the four month period and used only for illustrating the various fields and parameters used in the research program.

## 3. THE CLEAR AIR TURBULENCE STUDY

Clear air turbulence (CAT) is a microscale phenomenon (less than 2 kilometers in horizontal extent) but the conditions which are symptomatic of its existence are of snyoptic scale. Therefore, synoptic scale parameters may be used to determine areas where CAT could occur, that is forecasting areas where there is a high probability of CAT.

From various reports and their contradicaions it appears that no single parameter can detect CAT. Certain parameters can detect the possibility of CAT in some synoptic situations but fail in others.

The approach used in this paper was to take statistical studies made by previous investigators and to use the basic parameters which they related to CAT (2,3,5,7,8). If the magnitude of any one parameter becomes large or the sum of various parameters becomes large then there is a high probability of CAT in that area. Therefore, the problem is not one of forecasting actual CAT but rather to forecast areas of high and low probability of encountering CAT. In this way flights may be planned so as to expect least CAT.

The research program consisted of computing the equations shown in Appendix A. These equations were computed using the CDC 1604 digital computer. The program was written utilizing symbolic coded relocatable assembly program (SCRAP). It was necessary to use fixed point fractional numbers in order that Fleet Numerical Weather Facility (FNWF) subroutines could be used. All finite differences were computed using standard FNWF mesh length of 381 kilometers true at 60 degrees north latitude. There are no time derivatives in the program. The research reported here is accomplished using analytical fields. Operational use would employ

cast fields were used in this research. "Proc 24 hours print to the bottom of each field represents the practical forecast introal to be used operationally.

The research program was written to compute CAT in three layers

500 to 300, 300 to 200, and 200 to 100 millibars. Computations were

not made for the third layer since 100 millibar fields were not available.

The research program was written to compute on the entire 63 x 63 FNWF grid of the northern hemisphere. A boundary condition of zero was used for the outside rows and columns. The print routines are 22 x 22 extracts of the United States starting at FNWF grid point J008, I018. The latitude and longitude coordinates of the four corners of the printed fields starting with the lower left corner proceeding clockwise are: 9.1N 109.5W, 44.5N 165..W, 57.7N 3.1E, 13.0N 58.8W.

All printed fields are pure numbers and have no dimensional meaning. All scaled outputs have been shifted to the left end of the register and the first three numbers with sign bit are printed out in decimal. Grid points can take on values from -999 to +999 except those fields which have been made all positive. The decimal point does not appear on the printed fields. Therefore, the printed grid point values are from -999 to +999.

In the research program the capital letters refer to the parameter as computed from the data. The small case letters serving as exponents represent the number of times and direction the register has to be shifted in order to place the significant portion into the first three numbers. Therefore, the two with exponents represent the scaling coefficient. Since the computations were in fixed point fraction ! all

printouts had to be shifted so as not to exceed one at any grid point in the field. Exceeding one would result in a meaningless value at that particular grid point. In addition the entire field had to be kept large enough so that patterns could exist and not be at or near zero throughout the field. Since these fields are summed they must be small enough so as not to cause the summation field to exceed one at any grid point.

The research program was run for thirty-six days during December 1964 and January, February, and March 1965. The thirty-six days were chosen because they were the most active in CAT reports during the four month period. In other words, there were more reports by pilots encountering CAT on these particular days. In order to show an example of each field printed out by the research program the time 00Z 23 FEB 65 was arbitrarily selected. These fields appear in Appendix C. Each field was produced by an individual term which will be described as follows:

## THE FIRST TERM OF THE RESEARCH PROGRAM (APPENDIX A)

The First Term is 2<sup>a</sup> A where A is the Laplacian of absolute vortisity. When this term is negative there is a local maximum of absolute vorticity meaning it is larger at that grid point than the average of the surrounding grid points. Therefore, the cyclonic curvature or cyclonic shear or both are relatively large at that grid point. This should correspond to the cold side of the jet especially in throughs. According to Endlich and McLean (1) there is a greater percentage of CAT on the cold side of the jet. Also according to Harrison (2) there is a strong tendency for moderate to severe CAT to be associated with trough lines.

This term was computed for the layer by first calculating the absolute vorticity of the upper and lower level D fields. The Laplacian was then taken of each field and a vertical average made of the upper and lower levels to obtain the Laplacian of vorticity of the layer.

This parameter has depicted most of the CAT associated with the trough over the western United States. The severe CAT near New Orleans is in an area of very large negative numbers. The field is contoured at intervals of 100 with the origin at zero.

#### THE SECOND TERM

The Second Term is 2<sup>b</sup> B where B is the absolute value of the vertical change in the vector thermal wind. One of the parameters which Lake's (7) statistical testing indicated was associated with CAT was the vertical gradient of wind shear. As shown by Richardson (9) the thermal wind shear is proportional to the gradient of static stability.

The u and v components of the thermal wind were computed from the upper and lower level temperature fields. The difference between the upper and lower level values of the u component was found and each difference was squared. This was also done for the v component. The square root of the sum of the squared differences gives the magnitude of the vector difference. According to Endlich and McLean (3) the largest values of the thermal wind shear appear on the warm side of the jet. This was found to be true throughout the four months. The contour interval for this field is 25 and the origin is zero.

## THE THIRD TERM

The Third Term is  $2^{C}$  C where C is one half the geostrophic wind velocity squared. C therefore represents the specific kinetic energy or in other words the kinetic energy per unit mass.

Clem (2) found that most cases of moderate to severe CAT were associated with areas of isotach maxima.

This term was computed for the layer by calculating the u and v components of the geostrophic wind at the upper and lower levels. The upper and lower level u components were vertically averaged to obtain an average u component for the layer. The average v component for the layer was obtained by a similar process. The magnitude of the velocity squared is just the sum of the squared components.

In the research program this field is contoured at intervals of 100 with the origin at zero. Contoured at this interval the kinetic energy field clearly depicts the isotach maxima regions. The kinetic energy field in Appendix C shows this field depicting the CAT in the western part of the United States occurring in areas of relatively large wind speeds. The kinetic energy field fails to indicate the severe CAT near New Orleans because it occurs in an area of relatively light winds.

## THE FOURTH TERM

The Fourth Term is  $2^d\ D$  where D is the absolute value of the derivative of the kinetic energy with respect to pressure.

Lake's (7) statistical testing indicated that the gust intensities are related to the vertical gradients of horizontal kinetic energy.

This term was computed for the layer by first calculating the velocity squared at the upper and lower levels. The vertical gradient for the layer was then obtained by computing the difference between the upper and lower level values of the velocity squared. The absolute value was taken so as to have all values positive. CAT should be associated with

large values of this field. Large values of this field were found only in areas of large values of kinetic energy. This field was therefore redundant and was eliminated from the CAT forecast program. The contour interval was 100 with the origin at zero.

#### THE FIFTH TERM

The Fifth Term is 2<sup>e</sup> E where E is the absolute value of the Laplacian of kinetic energy. The statistical survey made by Endlich and McLean (3) shows the maximum occurrence of CAT along the edges of the isotach maxima. The Laplacian of kinetic energy shows large horizontal changes in kinetic energy, both positive and negative. Therefore the absolute value of the term is taken in order to give only positive numbers. The contour interval was 25 with the origin at zero.

This term was introduced to depict the areas of large horizontal change in kinetic energy. However, there was no relationship with reported CAT. This field was therefore eliminated from the CAT forecast program.

#### THE SIXTH TERM

At this point in the research program it was necessary to sum the first five terms due to computer memory space. This term, referred to as KAT1, was the Sixth Term. The contour interval was 250 with the origin at zero. It was found that this term did not supply significantly new information since it was dominated by the kinetic energy and the two associated terms.

#### THE SEVENTH TERM

The Seventh Term is  $2^f$  F where F is the Jacobian of temperature and omega (component of the wind normal to the pressure surface). This

term was developed by Dr. Moore of Douglas Aircraft and Dr. Krishnamurti (8). The latter was associated at that time with the University of California, Los Angeles and consultant to Douglas Aircraft. The term was developed as the Jacobian of temperature and three dimensional divergence. As shown in their paper this is proportional to the negative of the Jacobian of temperature and omega. This term was computed for the lower level of each layer in the research program. The contour interval for this term was 100 with the origin at zero. In this program no significant relationship was found with large negative or positive numbers over the four month period. This term was therefore eliminated from the CAT forecast program.

## THE EIGHTH TERM

The Eighth Term is 2<sup>g</sup> G where G is the absolute value of horizontal divergence. It was computed by taking the derivative of omega with respect to pressure. As previously stated the entrance and exit regions of isotach maxima areas have been found to be associated with CAT. These areas are also associated with horizontal convergence at the entrance and divergence at the exit regions. Therefore the absolute value of the change in omega with pressure represents the convergence and divergence in the layer parallel to the pressure surfaces.

This term was computed by subtracting the lower level omega value from the upper level omega value at each grid point. Areas of convergence and divergence of the height field are quite vividly depicted by the divergence field. No significant relationship was found between the divergence field and the CAT occurrences, therefore, it was eliminated from the CAT forecast program.

#### THE NINTH TERM

The Ninth Term was KAT2, the summation of all previous terms. No significant relationship was found with CAT occurrences since several terms tended to cancel each other out.

The program then goes into the second layer from 300 to 200 millibars. All terms were computed and scaled the same, except the divergence term. It could not be computed because the 200 millibar omega field was not available.

The third layer from 200 to 100 millibars could not be run for these time periods since the 100 millibar fields were not available.

There were very few CAT reports above 200 millibars, therefore, the loss was insignificant.

In all three layers the lower level height field is printed out first. This gives a general impression of the synoptic situation and renders more significance to the patterns developed in the other fields. The contour interval for the 500 millibar field is 60 meters with the origin at 5580 meters. The contour interval for the 300 millibar field is 120 meters with the origin at 9120 meters. The contour interval for the 200 millibar field is 120 meters with the origin at 11,760 meters.

The CAT forecast program appears in Appendix D. The first three terms of the research program are used with minor changes. In the first term "a" is changed to minus one and the contour interval has been changed to 150 to give better defined patterns. The second term has been used unchanged. The third term is unchanged except for the contour interval which was changed to 50 to increase the pattern size. The KAT field itself is the summation of these three terms and gives quite reasonable patterns and pattern sizes.

The pattern area depicting a high probability of CAT would necessarily be larger during a more active CAT period. The most active part of the year was the four month period December 1964, January, February, and March 1965. During these months the most active three day period was the tenth through the twelfth of March 1965. Therefore the KAT fields have quite large pattern sizes in Appendix E since they represent the most active three days of the year. The KAT field patterns were smaller for less active periods. The total area covered by these patterns is much less in the KAT field than in the other three parameter fields.

This is exactly what was attempted in order to obtain optimum size of the forecasted danger areas. If the KAT field patterns are too large, flights will be rerouted unnecessarily. On the other hand, if the KAT field patterns are too small, there is a real danger of CAT occurring outside these areas. Therefore, the restraint of the KAT field patterns is necessary in order to have an operationally useable product.

## 4. DISCUSSION AND RECOMMENDATION FOR FUTURE STUDIES

The period used in this paper was chosen because of the largest number of reported CAT occurrences. Of the four month period (December 1964, January, February and March 1965) there were scattered periods where a large number of occurrences were reported. This four-month period was used to determine which parameters were best suited for forecasting purposes. The three-day period of 10-12 March 1965 was selected for a correlation study in order to find out how successful our forecast method is. Tables 2, 3, and 4 show the various fields used and the resultant KAT field for the 10<sup>th</sup>, 11<sup>th</sup> and 12<sup>th</sup> of March 1965.

The use of the term "percent correlation" as used in this study does not mean to imply a statistical correlation. The ideal forecast verification makes use of those cases where CAT is forecast, but does not occur, and where CAT is not forecast and does not occur. In our study it was impossible to take those cases quantitatively into account. Therefore, it is to be understood that "correlation" as used in this study was a general comparison of those reported CAT occurrences that fell within the delineated area of high probability of CAT against those that did not. For example, if there were ten reported CAT occurrences for a given layer and time period and six of these reports fell inside or on the line delineating the CAT area and four reports fell outside the area, then for that field, layer and time period we would list it as six occurrences correlated or a sixty percent correlation.

Listed are the names of the fields, the number of occurrences of CAT for each field and the percent correlation by field. Also shown are the number of occurrences and the number of occurrences that correlated by field and CAT intensity.

After combining the Laplacian of Vorticity, Vertical Gradient of Thermal Wind and Kinetic Energy we arrive at the KAT Field which is our end product for the area of high probability of CAT occurrences. Even though a higher correlation may be seen in some fields other than the KAT field, one should realize that these fields encompassed a larger than average area. In such cases one must expect a high correlation.

The high correlation is then not due to the finesse of the forecast method, but rather due to the fact that for most of the USA there was a forecast of high probability for CAT. Theoretically, it would be a good idea to divide the percent correlation (such as we computed) by the size of the area for which CAT was forecasted. We did not follow this idea quantitatively, but only qualitatively. Therefore, one finds that the percent correlation for our ultimate forecast (labeled KAT) is sometimes lower than the percent correlation for one of the three separate forecasting fields.

Table 5 is a summary for the three day period. It shows the total number of CAT occurrences by turbulence category, percent correlation by field and turbulence category, and the three day percent correlation by field.

The results were most encouraging and we feel that our end product was a substantial step in at least the right direction toward forecasting clear air turbulence. Our knowledge of the meso- and micro- structure of flow patterns in the free atmosphere, especially above the tropopause, is still rather poor. A strong need still exists for a well organized and well equipped measurement program, especially at flight levels of the future supersonic transport aircraft. Measurement programs using

methods of data collection other than aircraft should be sought in order to obtain more information on the real micro- structure of the atmosphere, without the large disturbances which a flying aircraft will create itself.

Case studies of CAT occurrences so far were limited to a comparison of turbulence location with atmospheric parameters measured as closely as possible to the time of occurrence. We might gain some additional information on the physical causes of CAT if the development and previous history of flow patterns bearing CAT were studied.

There still exists a need for sensitive, accurate and compact instrumentation, especially an accelerometer which measures and records the three components of gustiness separately and simultaneously.

In summarizing we would like to state that turbulence research in the free atmosphere has come a long way, especially when we consider the fact that measurements are most difficult to duplicate in controlled experiments. We need the free atmosphere above us to conduct our research, and this same atmosphere has an infinite choice of parameter combinations. This should provide the seed of interest to combine the efforts of physics, aerodynamics, mathematics, statistics and meteorology to seek out and find a more complete and more satisfying solution of the problem.

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6. APPENDIX A EQUATIONS

The numbers in parentheses on this and the following pages refer to the page numbers in the text where each item is discussed.

The numbers below each term in the following two equations identify the number of each term (e.g., KAT1 is the sixth term).

THE RESEARCH PROGRAM (p. 15)

THE FIRST TERM 2<sup>a</sup>A (p. 15)

$$a = 0$$
  $A = \nabla^2 \eta$   $\eta_0 = f + \frac{g}{fd^2} [Z_1 + Z_2 + Z_3 + Z_4 - 4Z_0]$ 

$$\nabla^{2} \eta_{0} = \frac{1}{d^{2}} \left[ \eta_{1} + \eta_{2} + \eta_{3} + \eta_{4} - 4 \eta_{0} \right] \qquad \qquad \nabla^{2} \eta = 1/2 \left[ \nabla^{2} \eta_{u} + \nabla^{2} \eta_{L} \right]$$

THE SECOND TERM 2<sup>b</sup>B (p. 16)

$$b = 0 B = \left| \frac{\overrightarrow{\Delta v}}{\Delta P} \right|$$

$$U_{t} = \frac{-g}{fT} \left[ \frac{T_{2} - T_{4}}{2d} \right] \qquad \qquad V_{t} = \frac{g}{fT} \left[ \frac{T_{3} - T_{1}}{2d} \right] \qquad \qquad \overrightarrow{V}_{t_{u}} = U_{t_{u}} \mathbf{i} + V_{t_{u}} \mathbf{j}$$

$$\vec{v}_{t_L} = v_{t_L} \cdot v$$

$$\frac{\Delta \vec{V}_{t}}{\Delta P} = \frac{\begin{bmatrix} U_{t_{L}} - U_{t_{u}} \end{bmatrix}}{\Delta P} i + \frac{\begin{bmatrix} V_{t_{L}} - V_{t_{u}} \end{bmatrix}}{\Delta P} j = \frac{\Delta U_{t}}{\Delta P} i + \frac{\Delta V_{t}}{\Delta P} j$$

$$\left|\frac{\Delta V_{t}}{\Delta P}\right| = \left(\frac{\Delta U_{t}}{\Delta P}\right)^{2} + \left(\frac{\Delta V_{t}}{\Delta P}\right)^{2}$$

THE THIRD TERM 2°C (p. 16)

$$c = 0$$
  $C = \frac{\overrightarrow{V}}{2}^2$ 

$$U_g = \frac{-g}{f} \left[ \frac{Z_2 - Z_4}{2d} \right]$$

$$V_g = \frac{g}{f} \left[ \frac{Z_3 - Z_1}{2d} \right]$$

$$\overline{U}_{g} = \frac{U_{g_{u}} + U_{g_{L}}}{2} \qquad \overline{V}_{g} = \frac{V_{g_{u}} + V_{g_{L}}}{2}$$

$$\vec{v}_{g} = \vec{v}_{g}i + \vec{v}_{g}j \qquad \qquad \vec{v}_{g}^{2} = (\vec{v}_{g})^{2} + (\vec{v}_{g})^{2}$$

THE FOURTH TERM 2<sup>d</sup>D (p. 17)

$$d = 1 D = \left| \frac{\Delta \frac{\overrightarrow{V}^2}{2}}{\Delta P} \right|$$

$$\frac{\vec{\Delta V}^2}{\Delta P} = \frac{\vec{V}_L^2 - \vec{V}_u^2}{\Delta P} \qquad |\frac{\vec{\Delta V}^2}{\Delta P}| = \sqrt{(\frac{\vec{\Delta V}^2}{\Delta P})^2}$$

THE FIFTH TERM 2<sup>e</sup>E (p. 18)

$$e = 1$$
  $E = |\nabla^2 \frac{\overrightarrow{V}^2}{2}|$ 

$$\nabla^{2} \overline{\dot{v}}_{0}^{2} = \frac{1}{d^{2}} \left[ \overline{\dot{v}}_{1}^{2} + \overline{\dot{v}}_{2}^{2} + \overline{\dot{v}}_{3}^{2} + \overline{\dot{v}}_{4}^{2} - 4 \overline{\dot{v}}_{0}^{2} \right] \qquad |\nabla^{2} \overline{\dot{v}}_{0}^{2}| = \sqrt{(\nabla^{2} \overline{\dot{v}}_{0}^{2})^{2}}$$

THE SIXTH TERM (p. 18)

$$KAT1 = \nabla^2 \eta - \left| \frac{\Delta \overrightarrow{V}_t}{\Delta P} \right| - \frac{\overrightarrow{V}^2}{2} - \left| \frac{\Delta \overrightarrow{V}^2}{\Delta P} \right| - \left| \nabla^2 \frac{\overrightarrow{V}^2}{2} \right|$$

THE SEVENTH TERM 2<sup>f</sup>F (p. 18)

$$f = 11$$
  $F = J[T, \omega]$ 

$$J[T, \nabla_3 \cdot \vec{V}] = \frac{-1}{\gamma P} J[T, \omega]$$

$$J[T,\omega] = \frac{1}{4d^2} [(T_3 - T_1) (\omega_2 - \omega_4) - (T_2 - T_4)(\omega_3 - \omega_1)]$$

THE EIGHTH TERM 2<sup>g</sup>G (p. 19)

$$g = 13$$
  $G = \left| \frac{\Delta \omega}{\Delta P} \right|$ 

$$\frac{\Delta \omega}{\Delta P} = \frac{1}{\Delta P} \left[ \omega_{L} - \omega_{u} \right] \qquad \qquad \left| \frac{\Delta \omega}{\Delta P} \right| = \frac{1}{\Delta P} \qquad \sqrt{\left( \omega_{L} - \omega_{u} \right)^{2}}$$

THE NINTH TERM (p. 20)

$$\text{KAT2 = KAT1 + 2}^{11} \text{ J[T,}\omega] - 2^{13} \left| \frac{\Delta \omega}{\Delta P} \right|$$

PROG KAT PROGRAM (p. 20)

$$KAT = 2^{-1} \nabla^{2} \eta - \left| \frac{\Delta \overrightarrow{V}T}{\Delta P} \right| - \frac{\overrightarrow{V}^{2}}{2}$$

7. APPENDIX B

THE RESEARCH COMPUTER PROGRAM

KAT FUR CAST BEGLISTERING PROGRAM	COMPUTES 503 TO 330 MB LAYER	PUT DATE TIME IN A REGISTER	READS PACKED LOWER LEVEL D FIELD INTO	r n L	UNPACKS LOWER LEVEL D FIELD INTO FS1	READS LOWER LEVEL TEMPERATURE FIELD	501	UNPACKS LOWER LEVEL TEMPERATURE FIELD		READS PACKED UPPER LEVEL D FIELD INTO	404	UNPACKS UPPFK LEVEL D FIELD INTO FSO	READS, UPPER LEVEL TLMPERATURE FIELD IN	10 154	UNPACKS UPPER LEVEL TEMPERATURE FIELD	LNIC F32	REWINDS TU 3 CH 5/6		PRINTS LOWER HEIGHT FIELD	GENERATLS SINE FIELD STUMS IN FS4	CCMPUTES VORTICITY FIELD FROM UPPER	LEVIL U FIELU SIUMS IN FSS	COMPUTES YORTICITY FIELD FROM LOWER	LEVEL D FIELD STUMS IN 130	COMPUTES LAPLACIAN OF UPPER LEVEL VORT	ICITY FIELD SIDMS IN FOL
ETTPL MURGAN	67.43	IIME	K+ ADD2		UNPCKD2	READIZ		UNPCKT2		READDI		UMPCK01	RFAD 11		UNPCKFI		REWIND	REWINDI	PRINT	SINF	VURTISI		VGRT1S2		LAPLACI	
IDENE	585	SIA	ZIX		p 1.3	- 1. I.		217		- 1 a		РГЈ	J. F.		.₹TJ		PTJ	RIJ	ктл	2 [J	R I J		£1.9		610	
			START		+	+		+		+		+	+		+		+	+	+	+	+		+		+	
Course to the	00000 1 05 00000	20 0 02001 50 0 0000	75 4 90723	50.00.000	75 4 90726 50 0 90300	75 4 00746	50 0 00000	75 4 03754	56 0 00000	15 4 00705	00000 n 34	75 4 00713 50 3 00000	75 4 00733	50 0 00000	75 4 00741	SC 0 00000	75 4 00761	75 4 00765 50 5 00000	56 6 00060	75 4 00771 50 0 00000	75 4 00774	50 0 000 <b>co</b>	15 4 01301	56 y 00000	75 4 01)06	50 U 00000
00000		00900	16900		30900	50603		00604		00900		90900	00900		01900		00611	00612	0.0613	C0614	60615		20616		00617	

PAGE	COMPUTES LAPLACIAN OF LOWER LEVIL VORT	CCMPUTES AVERAGE VORTICITY BETWEEN UPPER A'10 LCWER LEVILS STOWS IN FSS		STOWS SCALED MAP FACTOR IN FS6	CCMPUTES U COMPONENT OF THERMAL WIND AT LOWER LEVEL STOWS IN FSO	COMPUTES U COMPCNENT OF THERMAL WIND AT LOWER LEVEL STOWS IN FS1	COMPUTES U COMPUTENT DIFFERANCE RETWEEN UPPER AND LUMER LEVELS STOWS IN FSO	COMPUTES V COMPGNENT OF THERMAL WIND AT LOWER LEVEL STOWS IN FSI	COMPUTES V COMPONENT OF THERMAL WIND AT UPPER LEVEL STOWS IN FS2	COMPUTES V COMPONENT DIFFERANCE BETAELM UPPER AND LIMER LEVELS STOWS IN ESI	COMPUTES VERTICAL GRADIENT OF THE MAL WIND STUNS IN FSO		HCRLZ MINUS DTHM STOWS IN FSS	SEE ABOVE	SEE AROVF	SEE AROVE	SEE ABOVE	REMINDS TU 3 CH 5/6	
	LAPLAGE	11 HIN I Z	PRINTI	WHAT	UTHM1	UTHM2	DUTHM	VTHM1	VTH*2	ОVТНМ	DIHM	PP INT2	KATI	READD2	UNPCKD2	PEADD1	U*PCKD1	REWIND	REMINDI
	€ 1.3		E13	. Ta	l T J	613	R 1.J	£1.8	PLα	. T .	RIJ	P I.J	fla	£1.9	ΣIX	۲۲ کا ۲	71 %	F13	ETA
	+	•	+	+	+	•	+	+	•	+	<b>.</b>	+	+	+	+	+	+	•	•
MURGAN	25 4 61.34 50 5 30 60	2 -	. 4C	75 4 01027 50 0 00000	75 4 01.134	י או נ אוני	•	75 4 31076 56 1 001060	0 4 3	· 4	, 4 5	75 4 01517 5c 5 00550	56 9 66363	75 4 50720 56 6 60060	75 4 00726	50500 6 95	75 4 C0713 50 U 00369	75 4 09761 50 4 00300	75 4 00765
	0.60	1 2 900	0.0622	00623	Cu624	00625	20626	200627	06 30	16 900	00632	60633	00634	56900	00636	00637	0.6640	00641	25923

SEE ABOVE	SEE ABOVE	COMPUTES U COMPONENT OF GEOSTROPHIC	COMPUTES U COMPONENT OF GEOSTROPHIC WIND AT LCWER LEVEL STOWS IN FS3	COMPUTES AVERAGE U COMPUNENT STOWS IN FS2	CCMPUTES V COMPONENT OF GEUSTROPHIC WIND AT UPPER LEVEL STOWS IN FS3	CCMPUTES V COMPONENT OF GEOSTROPHIC WIND AT LCWER LEVEL STOWS IN FS.	CCMPUTES AVERAGE V COMPONENT STOWS IN (S)	COMPUTES V SQUARF STOWS IN FSO			COMPUTES LAPLACIAN OF KINETIC ENERGY STOWS I 4 FS6		STOWS PREVIOUS TERMS IN FSO		SEE ABOVE	SEE ABOVE	REWINDS TU 3 CH 5/6	READS OMEGA FIELD INTO FS4	UNPACKS LCWER LVL OMEGA INTO FS6
SINF	MHAT	UGEOS1	UGEOS2	UGEOS	VGEUSI	VGEOS?	VGEOS	KINETIC	PRINT4	PRINTS	LAPKIN	PRINT6	KAT2	PRINT	READT2	UNPCKT2	REWIND	RE AD 02	UNPCK02
2 8	7 2	Ĩ a	£13	кТJ	RTJ	RTJ	kTJ.	RTJ	ž 2	КŢЗ	RTJ	RTJ	RTJ	RTJ	кту	RTJ	8T3	RIJ	RTJ
•	•	+	+ *	*	+	+	*	*	+	+	+	+	+	•	+	+	+	+	+
75 4 00771 6000 6 02	75 4 31.27	75 4 01154 50 U 00UCD	56 0 00000	4 0	4 3	4 7	4 3	3 4 5	45	75 4 91613 50 0 00000	50 0 00000	40	75 4 01306 50 0 00000	75 4 91663 50 0 00000	50 0 00000	50 0 00000	50 5 00000	50 0 00000	75 4 01335
60643	C0644	50995	00646	00647	03990	00651	00652	00653	10654	00655	906 56	000 57	09900	00661	00662	69900	00664	29900	99900

PAGE 600	REWLAS TUZ CH 3/6	GEMPOSTE, THE SACCHIAN OF TEMPERATURE AND CPECAL STEWS IN FST	REAUS OVEGA FIELD INTO ES4	UNPACK'S UPPER LVL OMEGA INTO FSS		CGMPUTE, PORIZORTAL DIVERGENCE STOMS FS5	CCMPUTES ABSCLUTE DIVERS STOWS IN FS5			CCMPUTES VORTICITY DIFFERANCE PLUS	ENERGY UTFFERANCE PLUS THE CHANGE IN BLUETIC ENERGY PLUS KINETIC ENERGY BLUETIC FOREST PLUS KINETIC ENERGY	PLOS IN CIVERGENCE		CCMPUTES 300 TO 230 MB LAYER	COMPUTES 200 TO 100 MB LAYER	END JE STEERING PROJRAM USES OFF LINE	<b>-</b>							
	ALWIND1	MILLIRE	READO	UNPCKOI	RFWINDI	HURDVG	ABSDIV	PRINTE	PAINTS	KAT			PRINT	LAYER2	LAYER3			:	TINE	MAG 0.0	MAA 13038	FS4 READERR	RF ADD1	** 0*6
	flo	1	LT 3.	RT3	Ç1 %	613	£13	fla	170	7 2			PTJ	RTJ	L I S	STS		813	LUA	L L d C	IZ I	22	51.3	SLJ
	+	+	+	+	+	+	+	+	+	+			+	+	+	+		PEADD1	+	+	045 IH			UNPCK 1
MERGAL	71 4 30765 56 1 99169	75 4 01342 50 3 00000	7	75 4 01322 50 0 00000	40	75 4 31355 50 1 30505	75 4 91365 50 0 00000	75 4 01707 50 4 06969	75 4 01543 50 3 00000	75 4 01373		35 1 CC 100	75 4 01663 50 0 00J00	よう	75 4 31424 50 4 00900	76 a ccodo	90000 m 34	75 5 30 (6)	17 0 02 01	77 4 04231	56 3 02014 50 3 01300	15 3 44215	50,000 ± 35	15 0 00000 15 6 60000
	19900	23070	0.06 /1	22 900	60673	90674	CU675	60676	11903	00200			06701	00102	00103	CO764		50100	30708	20200	00710	Cu711	00712	Lt 713

	# H > 4	F55 2	WAR	UMPCKD1	:	TIME WAME 2	0 4 O	MAA 13008	F34 RFALERK	RE AND2	?*O	*+2 FS4	FS1 24538	WAB 7	UVPCK02	:	TIME NAMES	0.0 0.0	MAA 13008	FS4 RFADERP	RCADT1	9.0	*+2 FS4	FS2 24538
	Ti.	33	01.J	51.3	SEJ	LOA	9013		27	51.3	LINI INI	618	25	P T S	51.3	217	LOA	LIX	ZZ 1±	22 0 L	51.3	SLJ	LJ.	000
	+		+		RE ADD.	+	+				UNDCKU2	+		+		RL ADT1	+	+	нгент			UNPCKII	+	
MIRKA		06 3 65453			000	12 0 (270) 16 0 01743	4.0	9 02	0 44	75 9 00020 56 0 00000		75 0 00731 00 1 44215	27	47	-		シラ				000	75 0 00 100 50 6 00 000	Φ.I.	00 1 24215 50 1 02453
	00714	C6715	00716	06717	00720	C0721	00722	C0723	00724	00725	C0726	20727	00730	50731	C07 32	00733	00734	0.1735	98 206	78 760	07400	55741	00742	C0743

MAD 7	UHPCKF1	:	TIME NAME4	00 00 00	MAA 13608	FS4 READERR	READ T2	9*0	*+2 FS4	F53 24538	WAB	UNIPCKTZ	:	MAA 113368	KEWIND	WINDERR	:	M44 11236P	KEWIND1	WINDERR	:	SA1 FS4	SINF
212	51.3	175	100	C18	ZZ	ZZ	513	SLJ	SEJ	99	LINA	SLJ	SEJ	613	517	SLJ	SLJ	RIJ	513	SLJ	SLJ	RTJ	SLJ
		READIZ	+	+				UMPCK 12	+		+		REWIND	+	+	+	REWINLE	+	+	+	SINE	+	+
50 90 6 97 50 90 6 97 50 90 6 97	30	50 0 00000	12 3 62001	15 4 04231	50 y <b>U2</b> 514 50 0 01300	50 0 02007	75 1 90746 50 0 00060	75 y 00000 50 6 00000	75 9 90757	0 34	50 5 00007		75 0 00000 50 0 00000		75 3 00761 56 3 00000	75 : 02913 50 : 000000	00000 - 59 90000 - 59	75 4 92914	75 U 00765 50 U 00300		75 P. 09960 56 J. 20702	(C-2)	75 1 23771 51 1 0636h
Co744	0(745	99746	C0747	00750	15700	64733	00753	00754	09755	00756	1510	09760	00761	00762	00763	99200	00765	99200	19700	06770	06771	00772	00773

FIRGA

** (75 1	FNI SAR	PAIN TANG	FNI VURTERI	SLJ VURTISI	2 SLJ **	SAR LINE	FNI FNI FSS	FNI VURTER2 FNI SAH	SLJ VURTIS2	1 SLJ **	PTJ SAU On FS0	03 FSS 00 LAPERRI	RTJ SAH FNI SAD+248	FNI SAD+128	SLJ LAPLACI	2 SLJ **		00 FS6 00 LYPERR2	RTJ SAH FNI SAD+248	ENI SAD+128	SLJ LAPLAC2	SLJ **	LDA FSU,4
VURTIS	+				VORTIS	+				LAPLAC	+		+			LAPLACZ	+		+			HOKIZ	L00P1
63699 C 54	75 4 04611 50 4 44215	57 3 05015 50 3 54255	59 9 92311 59 0 94451	50 0 00000	75 0 00000 50 0 00000	75 4 64611	00	50 0 02012 59 0 04451	75 J 01001 50 U 00000	75 0 00000 50 0 00000	75 4 04423 00 0 05015	00 0 54055 00 0 02004	50 0 04447	50 0 04435 50 0 04435	75 9 91006 50 9 90009	೧೨	75 4 04423 00 0 14655	00 0 63715 00 0 02005	50			75 5 00000 56 4 00000	12 4 05.115 14 4 14655
72.00	67.100	00776	CU777	01000	01001	01002	01003	01004	01003	01006	20010	01010	01011	01012	C1013	01014	C1015	01010	01017	01020	01021	01022	01023

F\$5,4	76008,4 1000P1	HORIZ	:	SAJHATERP	FS4 FS6	SAH SAJ+78	SAJ+78 SAJ+7P	MHAT	:	SAH	1 NS 1 D1	UTHM1	0 FS0,2	_	F54,2	CONSTI	LUCATI	F\$2,3 F\$2,1	LOCAT2 CONST2	FS6,2		50 F F 1	:
STA	SEJ	C 18	217	000	22	S S S S S S S S S S S S S S S S S S S	ZV	SLJ	SLJ	200 000	IN IN	517	FNA STA	SLJ	LEA	ADD	NUF ST∧	L DA S UB	STA	7 U Y U Y U Y U Y U Y U Y U Y U Y U Y U	DVF	STA	SLJ
	+		MHAT	+		+			LTHMI	01F1	+	+	CUTSTB1		IMSIDI								UIHMZ
20 4 54 55 56 5 60305		75 2 61922	7.0	40	2.2	4.5	0 045	75 0 01027 50 0 00000	00	75 4 94451 90 0 01041	56 9 01943 50 6 01943	20		0 010 0 000	2 444	2. [62]	017	3 2451 1 2451	0 017	2 6371	2 245	75 0 01136	75 11 000.00 50 1 100.00
1624	1025	1026	1027	1030	1601	1032	1033	1034	31035	31036	1037	1040	11041	1042	01043	01044	1045	11046	1047	35013	01051	7501	51053

MIRGAL

SAH OUTSID2	IMS102 IMS102	ОТНМ2	0 FS1,2	01F2	FS4,2	CONSTI LOCATI	LUCATI	FS3,3 FS3,1	LUCAT2 CUNST2	FS6,2 LOCAT2	LUCAT1 FS3,2	FS1,2 DIF2	**0	FS0,4 FS1,4	•	76008,4 L00P4	DUTHM	:	SAH OUTSID3	[45103 INS103	VIHMI	0 FS1,2	01F3
LO.	E NII	SLJ	FNA	513	LUA	ADD STA	MUF	LUA SUB	STA	Y U Y TU H	DVF DVF	STA	SLJ	L DA S UB	STA	I SK SLJ	SLJ	SLJ	RTJ	EZZ ZZ	SLJ	FNA STA	SLJ
01F2	+	+	0015162		INS102								DUTHM	L00P4		+		VTHM1	DIF3	+	+	0018103	
61 157	01361	01053	00000- 14655	01054	44215	01733	01775	34355 34355	01776	63715	01775	14655	00000	05015 14655	05015	07600	01071	00000	04451	01104	01276	00000 14655	01077
4.	7 -	عد	20	22	27	20	00	2		20	20		04		40		0.0	30	40		0.5		O T
1054 (5		1056 75	57 1	1060 75	61 1 U	1062 14	1063 26	1064 12 15	01065 20	1066 26	C1067 27	01070 20	01071 75	01072 12	01073 20	01074 54	01075 75	01076 75	1077 75 00	1100 50	11011	02	103 75
01	010	010	010	010	010	010	010	010	010	01(	010	010	010	010	CI	01	01	010	010	C1	01	C11	011

F54+2	CUTSTI	LUCATI	FS2+1,2 FS2-1,2	LOCAT2 CRINST2	F56, 2		SI	<u>د</u> *	SAH OUTSI64	16.5104 17.5104	VTHM2	2	DIF4	F54,2	STA	LUCATI	F53+1,2 F53-1,2	LUCAT2 CONST2	CA	CCAT S3,2	-5		F52,4 F51,4
L P.A. ARS		MUF	1 DA SUB	STA	₹UF UFI	PVF FVF	STA	SEJ	Fo ¥.	TE NE		SIA	SLJ	LDA	ADD STA	⊃ <b>⊢</b>	LDA	-0	FUF WUF	UVF	STA	SL N	LDA
105103								ZWH1V	C1F4	•	+	0015104		POISNI								СУТНМ	LONP7
2.5	31733 31775	11	24516 24514		63715	1-5	35	00000	4.4	112	0.10	000 451	110	44215 00301	25	~~	34356	51776 51734	63715		5	000000	24515 14655
12 2	2000	3 92 3 92	12 5						75 4													75 1	
01104	01105	01106	01107	c11110	C1111	01112	01113	011114	01115	011116	C1117	01120	11121	01122	01123	C1124	01125	C1126	01127	01130	01131	01132	C11 33

FS1,4	76008,4 L00P7	DVIHM	** 0 * 4	FS0,4 FS0,4	FSU,4 FS1,4	FS1 ,4 FS0,4	VAB SOERR	FS0,4	76008,4 LOOP8	ОТНМ	** 0,4	FS5,4 FS0,4	FS5,4	76008,4 L00P9	KAT1	*	SAH OUTSI05	145105 1NS105	UGEOS1	0 FS2,2	01.65	FS4,2	CUNSTI
STA	1SK StJ	SEJ	SLJ	LEDA	STA	A DD	RTJ	5 T A	1SK SLJ	SLJ	SLJ	LDA	STA	I SK SLJ	SLJ	51.3	617 00	NN NN	SLJ	FNA	SLJ	LDA	ADD STA
	•		OFHR	L00P8			+	+	+		KAT1	L00P9		•		UGEOST	DIES	+	+	PUTS105		OISNI	
14655 00000	07600	01132	00000	05015	05015	14655	94666	95315 66 104	77500 011140	01137	000000	54055 05015	54055	02110	000000	000000	04451 91160	01162	01154	00000 24515	01155	44215	01733
40	40	S/ D	4	44	44	44	40	5 -	4.5	10	04	44	40	40	さつ	30	40	7.0	20	~~	22	د. ۲	30
2004	54		75	12 26	20	26 14	125	250	54	200	50	12	20	54	305	200	75	50	75	10	75 50	12 01	40.7
61134	01135	01136	01137	01140	01141	01142	01143	01144	01145	011146	01147	01150	01151	01152	01153	01154	01155	C1156	01157	0110	01161	C11 62	¢1163

WUF LUCATI	DA UE	STA LUCATZ	MUF FS6,2	0VF LUCAT1 STA F52.2	J 01F	SLJ **	STJ SAH		SEJ UGEOS2	6 ENA 0 FS3.2	SLJ DIF6	LDA F54.2 ARS 1	ADD CONSTI	MUF LOCATI	LDA FSI,3	STA LUCATZ LDA CUNSTZ	MUF ES612	STA FS3,2	LJ DIF	**************************************	16A F52,4	STA LCCATI	ALS 3 ADD LOCATI
20.00	ιντ	94	\$2	a.v.	22	0 006052	1 01F6	+	+	0 001510	mo	5 145106	സ	vuv.	S	4	65	5.5	mc mc	0 UGEOS	5 LOOP13	r. rv	~w
C177 0177	0501	177	6371	2451	01155	0000	044	0120	0117	9636	0000	4421	0173	7710	1465	0177	6371	3435	0000	0000	2451	3435	900C
26 0 20 1	12 3		26.2 26.0		75 0		75 4 00 0						14 J 20 0	90	12 3 15 1	00	26 2 7 26 2	~0	50	75 0	12 4	20 0 12 4	14 7
31164	11165	99110	11167	011170	17113	21112	51173	01174	51110	01176	77110	01200	01201	01202	01203	01204	01205	01206	01207	01210	01211	01212	01213

MURGAY

F52,4	76.00B,4 LOGPI0	UGFOS	:	SAH OUTSID7	INSID7 INSID7	VGEUS1	9 FS3,2	0167	FS4,2	CONSTI	LOCATI	FSO+1,2 FSO-1,2	LUCAT2 CONST2	FS612 LOCAT2	LOCAT1 FS3,2	DIF7	*	SAH OUTSID8	INSID8 INSID8	VGEOS2	0 FS0,2	01F8	FS4,2
SIA	1 SK SLJ	SLJ	SLJ	LT. OC	MM NN NH	SLJ	ENA	SLJ	LNA	ADD	MUFSTA	LDA	STA	F U F U F U F U F U F U F U F U F U F U	DVF STA	517	SLJ	00 00	EN N N I I I	SLJ	ENA	SLJ	LDA
	+		VGEOSI	0167	+	+	0018107		LUSID								VGECS2	01F8	+	+	RUTS108		INS108
24515	07600	01210	000000	04451	01225	01217	34355	01220	44215	01733	01775	05016	01776	63715	01775	01220	000000	04451	01243	01235	00000	01236	44215 000001
200 4 500 5	54 4	200	20 00	50 5	000	50.00	2002	0 00	12 2 01 0	4000	30 30	2 5 5 1	20 C	26 2	20 2	20 00	50 0	75 4 00 00	SO 03	25 0	10 3 20 2	20 05	12 2
01214	01215	01216	C1217	01220	01221	01222	01223	61224	01225	C1226 1	01227	C123C	01231	01232	61233	01234	61235	01236	C1237	01240	(1241	01242	01243

CCNST1. LOCAT1	LUCATI	FS1+1,2 FS1-1,2	LUCAT2 CONST2		LCCAT1 FSG,2	ртев	**0	FS3,4	LOCATI FSU.4	LOCATI	FS0,4	Ca	VGEOS	**0	FS2,4 FS2,4	LOCATI FS0.4	FS9.4 LUCAT2	LOCAT1	FS0.4 LOCATI	LUCAT2 FS4,4	FS4,4 FS4,4	7600B34	KINETIC
ADD	F UF S TA	LOA	STA	N. S.	NVF STA	SLJ	SLJ	LDA	STA	ALS ADD	STA	I SK SLJ	SLJ	SLJ	LDA	STA	MUF STA	AND	STA	SUB STA	FUF	I SK SLJ	
							VGEOS	L00P11				+		KINETIC	L00P12							+	
01733	01775	14556	01776	63715	01/75	01236	00000	34355 00003	01775	000003	05115	07600	01253	000000	24515	01775	05215	01775	5015	01776	44215	07669 01263	01262
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173	£ 5 0177	2 2 1455 5 2 1455	2 3 0177	2 6371	0 2 0501	0123	5 0 0000	4 3435	2 4 0501	00000	4 05J1 0 0090	4 0760 0 0125	0125	00000 2	4 2451	0 0177	6 0521 0 0177	0 0177	0 4 05015 2 6 01775	4421	4421	4 4 9760 5 0 0126	126

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01464	01465	01466	01467	01470	01471	01472	01473	01474	01475	01476	01477	01200	91501	01502	C1503	C1504	01505	01506	21507	01510	11511	21510	61513

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99210	01705	01706	01707	01710	01711	01712	C1713	01714	01715	91716	C1717	01720	01721	01722	01723	C1724	01725	01726	01727	01730	C1731	01732	01733

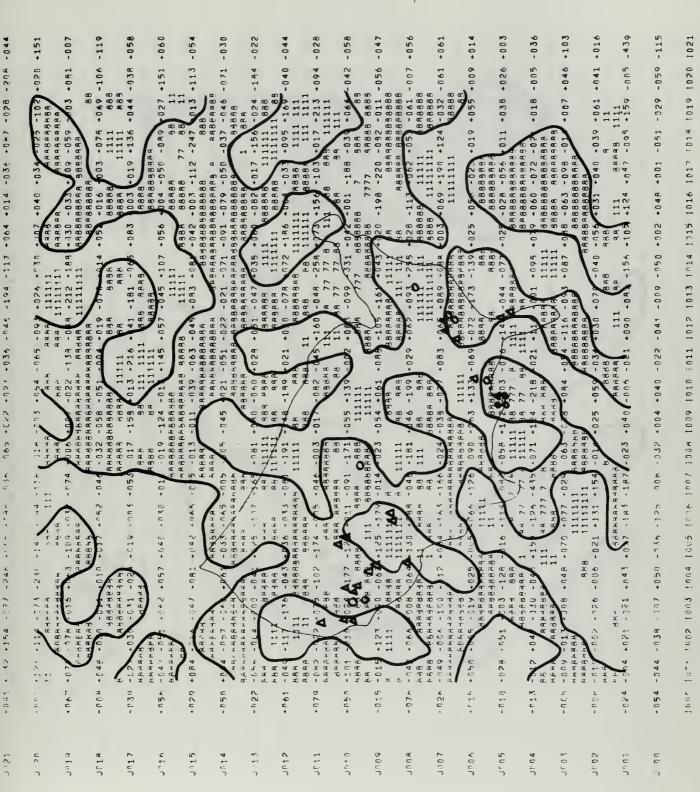
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02524 VAA 1.18 MAA	04231 MAC LIB MAC	04371 MAG LIB MAG	U4423 SAB LIB SAB	04451 SAD LIB SAD	04535 SAH LIB SAH	04570 SAI LIB SAI	04611 SAJ LIB SAJ	U4666 SAR LIB SAR	04715 VAB LIB VAB	04745 WAB LIB WAB	(15315 WAE LIB WAE	14655 FSO RSS 4000	24515 FS1 PSS 4,000	34355 FS2 BSS 4000	44215 FS3 PSS 4000	54355 FS4 RSS 4000	63715 FS5 8SS 4000	73555 FS6 RSS 4000	00000
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## 8. APPENDIX C

PRINTED FIELDS FROM THE RESEARCH PROGRAM FOR OOZ 23 FEB 65



00Z 23 FEB 65

24 HOURS

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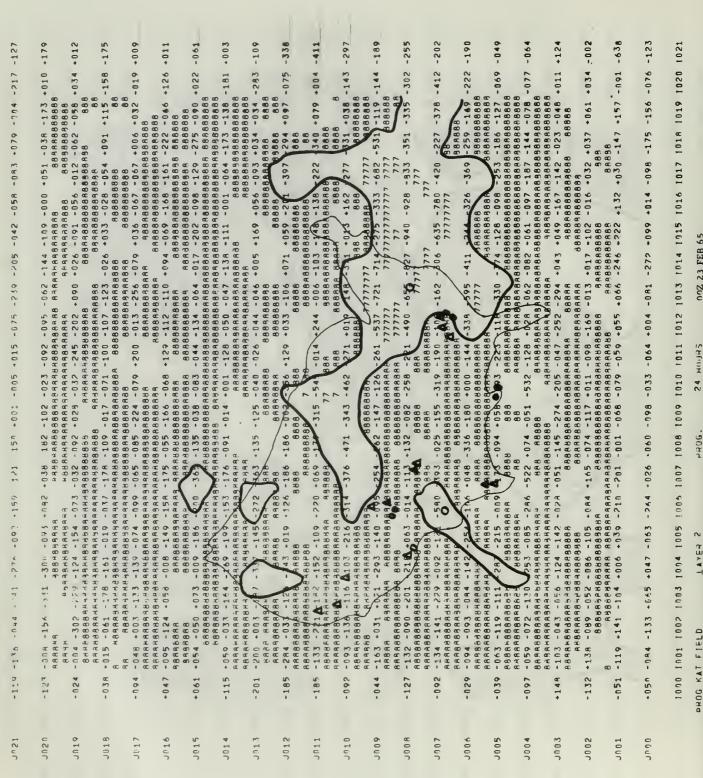
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LAYER 2

PROG KAT FIFLD



00Z 23 FEB 65

## 9. APPENDIX D

THE CLEAR AIR TURBULENCE FORECAST COMPUTER PROGRAM

KAT FORECAST GEOIN STEERING PROGRAM COMPUTES 503 TO 300 MR LAVER		PUT DATE TIME IN A REGISTER	READS PACKED LOWER LEVEL D FIELD INTO	ר	UNPACKS LOWER LEVEL D FIELD INTO FSI	READS LOWER LEVEL TEMPERATURE FIELD		UNPACKS, LOWER LEVEL TEMPERATURE FIELD	1810 133	READS PACKED UPPER LEVEL D FIELD INTO	77	UNPACKS UPPER LEVEL D FIELD INTO FSO	READS UPPER LEVEL TEMPERATURE FIELD IN		UNPACKS UPPER LEVEL TEMPERATURE FIELD	75. 0.11	REWINDS TU 3 CH 5/6	REWINDS TU 2 CH 5/6	PRINTS LOWER MEIGHT FIELD	GENERATES SINE FIELD STOWS IN FS4	COMPUTES YORTICITY FIELD FROM UPPER	LEVEL U TIELU SIONS IN F35	COMPUTES VORTICITY FIELD FROM LOWER	בריבר ה זורה זותה זות זות	COMPUTES LAPLACIAN OF UPPER LEVEL VORT		COMPUTES LAPLACIAN OF LOWER LEVEL VORT	17.
	8009	TIME	RE ADD2		UNPCKD2	READT2		UNPCKT2		RE ADD1		UNPCKDI	READT1		UNPCKT1		REWIND	REWINDI	PRINT	SINF	VORTISI		VORT IS2		LAPLACI	•	LAPLAC2	
	ORG	STA	RTJ		RTJ	RTJ		KIJ		RTJ		613	RTJ		RTJ		RTJ	RTJ	RTJ	RTJ	RTJ		RTJ		RTJ		RIJ	
			START		+	+		+		+		+	+		+		+	+	•	+	+		+		+		+	
	00900	20 0 01461 50 0 00990	4	50 0 00000	50 0 00.000	4	50 000000	75 4 00730	00000 0 05	4	20 0 00000	75 4 U0667 50 J 00J00	75 4 00707	C	75 4 00715	50 0 00000	40	40	50 3 00000	40	75 4 00750	50 0 00000	75 4 00755	20 0 00000	75 4 00762	20 0 00000	75 4 00770	50 0 00000
		00900	00001		00602	00003		900900		50900		90900	00000		00910		00611	00612	00613	00014	00615		91900		00617		00620	

COMPUTES AVERAGE LAPLACIAN BETWEEN	UPPER AND LOWER LEVELS STOWS IN FS5	PRINTS LAPLACIAN OF VORTICITY	STOWS SCALED MAP FACTOR IN FS6	COMPUTES U COMPONENT OF THERMAL WIND	LEVEL SIUMS IN	COMPUTES U COMPONENT OF THERMAL WIND	LUMER LEVEL STUWS IN	COMPUTES U COMPONENT DIFFERANCE BETWEEN UPPER AND LOWER LEVELS STOWS		COMPUTES Y COMPONENT OF THERMAN WIND	LEVEL STUMS IN	COMPUTES V COMPONENT OF THERMAL WIND	LEVEL SIUMS IN	COMPUTES V COMPONENT DIFFERANCE BETHEEM UPPER AND LOWER LEVELS FOUR	N FS1	COMPUTES VERTICAL GRADIENT OF	THEKMAL WIND STOMS IN FSO	PRINTS VERTICAL GRADIENT OF VT	HORIZ MINUS DTHM STOWS IN FS5	SEE ABOVE	SEE ABOVE	SEE ABUVE	SEE ABOVE	REWINDS TU 3 CH 576	REWINDS FU 2 CH 5/6	SEE ABOVE
HORIZ		PRINTI	MHAT	UTHM1		UTHM2		DUTHM		VTHM1		VTHM2		DVTHM		ртнм		PRINT2	KAT1	READD2	UNPCKD2	READDI	UNPCKDI	REWIND	REWINDI	SINF
RTJ		RTJ	RIJ	RTJ		RTJ		RTJ		RTJ		L1 d		RTJ		RTJ		RIJ	RTJ	RIJ	PIJ	RTJ	RTJ	RTJ	RTJ	RTJ
+		+	+	+		+				+		+		+		+		+	+	+	+	+	+	+	+	+
75 4 00776	50 0 00000	50 0 00000	50 0 00000	75 4 01911	20 0 00000	75 4 01027	50 U 00000	75 4 01045	20 0 00000	75 4 01052	26 0 00000	75 4 01070	20 0 00000	75 4 01106	50 0 00000	75 4 011113	20 0 00000	75 4 01343 50 0 00000	75 4 01123 50 0 00000	75 4 00574 50 0 00000	50 0 00300	75 4 00661 50 0 00000	50 0 00000	56 0 00000	50 9 00 00 50	75 4 00745 50 9 00000
006 2 1		00622	C0623	00624		00625		00626		00627		00630		00631		C0632		0.0633	00634	00635	96900	7 6 900	0000	00641	00642	00643

SEE ABOVE	COMPUTES U COMPONENT OF GEOSTROPHIC WIND AT UPPER LEVEL STOWS IN FS?	COMPUTES U COMPONENT OF GEOSTRUPHIC WIND AT LOWER LEVEL STOWS IN FS3	COMPUTES AVERAGE U COMPONENT STOWS IN FS2	COMPUTES V COMPONENT OF GEOSTROPHIC WIND AT UPPER LEVEL STOWS IN FS3	CCMPUTES V COMPONENT OF GEOSTROPHIC WIND AT LCHER LEVEL STOWS IN FS .	COMPUTES AVERAGE V COMPONENT STUMS IN FSO	COMPUTES V SQUARE STOWS IN FSO COMPUTES V SQ DIFF STOWS IN FS4	PRINTS KINETIC ENERGY FIELD	STOWS PREVIOUS TERMS IN FSO	PRINTS PROG KAT FIELD	COMPUTES 300 TO 200 MB LAYER	END OF STEERING PROGRAM USES OFF LINE PRINTING							
MHAT	USEOSI	UGEOSZ	UGEOS	VGEOSI	VGEUS2	VGEOS	KINETIC	PRINT3	KAT2	PRINT4	LAYER2		•	TIME	00 * 00 ° 00 ° 00 ° 00 ° 00 ° 00 ° 00 °	1300B	FS4 READERR	READDI	0.6
F 13	619	# <b>1</b> 2	P13	2	fl <sub>a</sub>	CT.	r L a	RTJ	813	6.1.3	RTJ	SLS	813	LDA	000	NZ UE	NN IN IN	517	SLJ
+	+	+	+	+	+	+	+	+	٠	+	+	+	READDI	+	*	нгенр			UNPCKUI
75 4 91 303	75 4 01130 50 4 00450	4 3	· • •	- 17 -	75 4 01211	4	75 4 01236	40	40	55 5 601411	75 4 01253 50 5 00050	76 J 00000 50 J 00000	75 0 00000 56 0 00000	12 0 01461	00000 0 000	50 0 01472	50 0 43641	50 9 00561	00000 9 05
90644	00645	00646	24900	26900	00651	000 52	00653	00654	00655	95 900	00657	006 60	00661	59900	00663	9000	0000	94900	24900

*+2 FS4	FS0 22538	-1 <u>E</u>	UNPCKOI	*	TIME NAME2	0 <b>8</b> 0	MAA 13608	FS4 RLADERP	READD2	# # D	.75° 44	F51 24538	WAB 7	UMPCKD2	# *	TEMP NAMES	MAG 0.0	MAA 13078	FS4 READE C	READT	****	*H*	FS2 2453P
SLJ 000	000	FNI	SLJ	SLJ	LDA	RTJ 000	ME NE	ZZ U.W	SLJ	SEL	SLJ 900	00	P.TJ ENI	SLJ	SLJ	L04 L00	RTJ DU	ZZ Ww	ZZ 20,	SLJ	SLJ	SLJ	
+		+		READD2	+	+				UNPCK02	+		+		READTA	+	+	нгент			UNPCKI	+	
75 0 00672	00 0 04441	3	200	50 0 00000	12 0 01461 16 0 01440	75 4 03707 00 0 00000	50 0 01472 50 0 01300	50 J 43641 50 J 01465	75 9 00674 50 0 00000	75 9 00000 50 6 00000	75 : 00705	000	40	75 0 00702 50 0 00000	75 y 900000 50 D 00000	12 0 01461	75 4 03707	50 0 01472	50 0 43641 50 0 01465	50 0 00360	75 0 00000 50 6 00000	75 0 00720 00 0 43641	00 0 24141 00 0 02453
0		0	00673	00674	92900	92900	22 900	00700	00701	00702	00703	00700	00100	90100	70700	00710	11	00712	00713	00714	00,715	00716	17

+ RIJ WAB	SLJ UNPCKTI	REAUTZ SLU **	+ LDA TIME LDQ NAME4	4 000 0 000 0 000 0 0 0 0 0 0 0 0 0 0 0	ENI MAA FNI 13008	FNI FS4 FNI READERK	SLJ RFADT?	UNDCKT2 SLJ **	+ SLJ #+2	00 FS3	+ KTJ WAB	SLJ UNPCKT2	REMIND SLJ +*	+ RTJ MAA	+ SLJ REWIND	+ SLJ WINDERR	REMINDI SLJ **	+ RTJ MAA	+ SLJ REWINDI	+ SLJ WINDERR	SINF SLJ **	+ RTJ SAI	+ SLJ SINF
4,000	50 0 00715	00	0 014	40	50 0 01472 50 0 01300	y 436 9 014	00	75 9 00000 56 6 00000	00073	00 0 34101	40	50 0 00000	50 0 00000	75 4 01472	00	55 5 00000	2000	35 4 01472	50 0 00000	50 0 00000	50 0 00000	75 4 04161 50 0 43641	50 0 00000
500	007.1	3 2 200	0072.3	00724	92700	06726	00727	00730	00731	00732	00733	00734	00735	95700	00737	03740	00741	00742	00743	00744	57100	95100	00747

SLJ **	RTJ SAR ENI FS4	FANI FASO FASO FASO FASO	ENI VORTERI	SLJ VORTIS1	St.J **	ENI SAR	FSI FSI FSI	ENI VORTERZ	SLJ VORTISZ	SLJ **	RTJ SAB	00 FSS LAPERRI	RTJ SAH ENI SAD+248	ENI SAD+128	SLJ LAPLAGI	\$LJ **		00 FS6 00 LAPERR2	RTJ SAH SAD+248	ENI SAD+128	SLJ LAPLAC2	SLJ **	LDA FS0,4 ADD FS1,4
VØR 1 [ 51	+				VORTI \$2	+				LAPLACI	+		+			LAPLAC2	+		+			HOR 12	L00P1
55 4 90100	75 4 04235	50 0 04441 50 0 53501	50 0 01467	50 0 00000	75 0 00500 50 0 00300	75 4 04235 50 0 43641	50 0 14301	50 0 01479	75 0 00755 50 0 00000	75 9 99969 50 9 99309	75 4 04047	00 9 53501	75 4 04075	50 0 04061 50 0 04061	50 0 00000	50 0 00000	75 4 04347	00 0 63341 00 0 01464	50 5 04073	50 0 04061 50 0 04061	50 0 00300	50 4 00000	12 4 04441 14 4 14301
05 205	00751	00752	00753	00754	00755	00756	00757	09200	19200	00762	00763	00764	00765	00166	00767	00770	00771	00772	90773	00774	30775	927700	77760

1 F>5,4	76008,4 LOOP1	HORIZ	:	SAJ	FS4 FS6	SAH SAJ+7B	SAJ+78 SAJ+78	MHAT	:	SAH	INSIDI	UTHMI	P.S.0.2	DIFI	F54,2	CONSTI	LOCATI	FS2,3 FS2,1	LOCAT2 CONST2	FS6AT2	-2	FSO,2 DIF1	:
ARS	1 SK SLJ	SLJ	SLJ	RTJ 00	NN NN	A DO	NN NN	SLJ	SLJ	000	N.A.	SLJ	ENA		LDA	ADD	STA	LDA	STA	AUT PU	DVF DVF	STA	SLJ
	+		MHAF	+		+			UTHM1	01F1	+	+	0015101		145101								UTHM2
20 4 53501	54 4 07600 75 0 00777	75 0 00776 50 0 00000	50	75 4 04214 00 0 01462	00	75 4 04975 50 5 04223	00	75 0 01063 50 0 00000	00	75 4 04075 50 0 01015	50 0 01317 50 0 01017	50	10 0 00000 20 2 04441	100	12 2 43641	14 0 01434 20 0 01455	26 0 01455 20 0 01455	12 3 24141 15 1 24141	20 0 01456 12 0 01435	26 2 63341 26 0 01456	27 2 24141	20 2 04441 75 0 01012	75 0 00000 50 0 00000
0.0013	1001	1007	1003	1004	1005	1006	1001	1010	1111	1012	1013	1014	1015	1016	1017	1020	1021	1622	1023	1024	1,025	1026	1027

SAH OUTSID2	INSI D2 INSI D2	UTHM2	P. 51,2	D1F2	F54,2	CONSTI	LOCATI	FS3,1	LUCAT2 CONST2	FS6.2 LOCATZ	LUCATI FS3.2	F51.2	0.4	FS0,4 FS1,4	FS0,4	75908,4	DUTHS	* *	SAH OUTSID3	INSIDA	VIHMI	0 FS1,2	D1F3
000	NN NN NN	SLJ	FNA	SLJ	LDA	ADD	MUF	LDA	STA	FUN FUN	DVE	STA	SLJ	LDA	STA	ISK	SLJ	SLJ	ST.	22 22	Sta	STA	SLJ
01F2	•	+	0015102		INSIDS								ООТНЯ	L00P4		+		VTHM1	01F3	+	+	0015103	
75 4 04075 00 0 01033	50 0 01035 50 0 01035	75 0 01027 50 0 00000	10 9 00000 20 2 14301	75 0 01030 50 0 00000	12 2 43641 51 6 00501	14 0 01434 20 0 01455	26 0 01455 20 0 01455		20 0 01456 12 0 01435			20 2 14301 75 5 01030	5 0 00	12 4 04441 15 4 14301	20 4 04441 50 0 00000		75 y 01045 50 0 00000	75 U 00000 50 U 00000	75 4 04075	50 0 01960 50 0 01960	75 J 01 J52 50 U 00 J03	10 0 00000 20 2 14301	75 0 01353 50 0 00000
01030	01031	01032	01033	01034	01035	01036	01037	01040	01041	C1042	01043	51044	01045	01046	01047	01050	01051	01052	01053	01054	(1055	01050	01057

LUA FS4,2	0-	MUE LUCATI	LDA FS2+1,2 SUB FS2-1,2	STA LOCATZ	UF FS6+2 UF LOCAT	DVF LOCATI	STA FS1,2	** 618	\$ 1	I INSTI	SLJ VTHM2	STA FS2,2	SLJ DIF4	LDA FS4,2	STA CONSTI	STA LOCATI	LDA FS3+1,2 SUB FS3-1,2	LDA CONST2	UF FS6AF	DVF LOCATI	A FS2, J DIF4	SLJ ** ENI 0,4	SUB FS1,4
1.45103								VT14M2	0164	+	+	0015104		1NS1D4	•							DVTHM	L00P7
2 43641	J 51434	014	2 24142 2 24140	01456	2 63341 2 J1456	2 24141	2 14301 0 01053	0000	70	0107	010	0 000000 2 24141	010	4364	01434	0145	2 34002 2 34000	0 01456	6334	0 01455 2 34001	2 24141 0 01071	000000 4 000000	4 24141 4 14301
01060 12	C1361 14						C1067 20 75					01074 10		C1076 12 31				01102 20			01105 20		01107 12

F51,4	76008,4	DVTHM	*00,4	FSU,4	FS0,4 FS1,4	FS1,4 FS0,4	VAE	F S 0, 4	76538,4 L00P8	ОТНМ	** 0*4	FS5,4 FS0,4	FS5,4	76008,4 L00P9	KAT1	:	SAH OUTSID5	INS 105 INS 105	UGE081	0 FS2,2	DIFS	F54,2	CONST1 LOCAT1
STA	1 SK SLJ	SLJ	SLJ	LDA	STA	MUF ADD	RTJ	SFA	1 SK SLJ	SLJ	SLJ	LDA SUB	STA	1 SK SLJ	SLJ	SLJ	RTJ 00	ENI	SLJ	STA	SLJ	LOA	ADD
	+		ОТНМ	LOUP8			+	+	+		KAT1	64007		+		USEUST	01F5	+	+	0018108		INSIDS	
50. 5. 14301.	54 4 07630 75 3 01107	00 00	56 4 00300	12 4 04441	4 10 4	26. 4. 14301 14. 4. 04441	5 4 04	21. 4. 34441 50. 1. 03.103	54 4 07600 75 0 01114	75 0 01113 56 0 000003	50 4 003000	4 5350	50 4 53501	54 4 97600 75 9 91124	9 011 9 000	00	75 4 04975 00 5 31134	0,011	00	0 2 2 2	5 5 5	12 2 43641	14 + 01434 20 -) 01455
01110	01111	01112	C1113	01114	01115	01116	011117	C112c	01121	01122	01123	C1124	01125	01126	01127	01130	c1131	01132	01133	01134	01135	01136	21137

LOCATI	F50,3 F50,1	LUCAT2 CONST2	FS642 LOCAT2	LOCAT1 FS2,2	01F5	:	SAH	INSID6 INSID6		0 FS3,2	0116	F54,2	CONSTI	LOCATI	FS1,3 FS1,1	LOCAT? CONST2	FS6+2 LOCAT2	LOCAT1 FS3,2	01F6	• 0	F52,4	LOCAT1 FS3,4	LOCATI
STA	LDA	STA	MUD	DVF	SLJ	SLJ	RTJ	ZZ ZZ	SLJ	FNA	SLJ	LDA	ADD	STA	LOA	STA	MUF	STA	_	SLJ	LDA	STA	ALS
						UGEOS2	DIF6	+	+	0015106		INSID6								UGEOS	C00P10		
01455	04441	01456	63341	01455	01131	000000	04375	01154	01146	34001	001147	43641	01434	01455	14301	01456	63341	01455	000000	000000	24141	34001	00003
20	e-1	20	20	90	00	00	40	50	00	90	00	20	00	00	~~	00	20	02	00	04	40	04	00
26 20	12	20	26 26	27 20	15	75	000	5.00 0.00	75	10	75	12 01	14 20	26	12	20	26 26	27 20	75			20	14
01140	01141	01142	01143	01144	01145	01146	01147	01150	01151	01152	01153	01154	01155	01156	01157	01110	19110	01162	01163	01164	9110	01166	01167

F52,4	7600B,4 LOCP17	UGENS	:	SAH OUTSID7	INSID7	VGEOS1	J F53,2	DIF7	FS4,2	CONSTI	LOCATI	FSO+1,2 FSO-1,2	LOCAT2 CONST2	FS6,2 LOCAT2	LOCAT1 FS3,2	DIF7	:	SAH	INSID8 INSID8	VGEDS2	0 FS0,2	0168	FS4,2
SIA	ISK	517	SLJ	RIJ	AT NE	SLJ	ENA	517	LDA	ADD	MUF	LDA	STA	MUF	OVE	SLJ	SLJ	000	MT NY NY	SLJ	STA	SLJ	LDA
	+		VGEOS1	0167	+	+	PUTS107		INSID7								VGEOS2	0168	+	+	0012108		INSTOB
50 4 24141	54 4 07630 75 0 01165	20	75 0 00000 50 0 00000	75 4 04075	50 0 01201	75 J 91173 56 J 96900	19 9 00309 29 2 34301	50 1 00000	12 2 43641 01 5 00001	14 ) 31434 23 3 01455	26 J 01455 20 J 01455	12 2 04442 15 2 04440	20 0 01456 12 0 01435	26 2 63341 26 0 01456	27 2 01455 20 2 34001	00	75 J 00300 50 0 00000	75 '4 04975 00 0 01215	50 0 01217	75 y 01211 50 y 00000	10 0 00000 20 2 04441	75 0 01212 50 0 00000	12 2 43641 01 J 00001
1170	01171	01172	01173	01174	01175	C1176	01177	01200	01701	01202	51203	01204	01205	01206	01207	01216	01211	01212	01213	61214	01215	01216	01217

CONSTI	LUCATI	FS1+1,2 FS1-1,2	LUCAT2 CONST2	FS6,2 LUCAT2	FSO.2	0168	4.0	FS3,4	LUCAT1 FS0,4	LOCATI	F50,4	760081 LOOP11	VGEOS	<b>**</b> 0 <b>**</b>	FS2,4 FS2,4	LOCAT1 FS0,4	FS044 LOCAT2	LOCATI	FS0,4	76008,4 LOOP12	KINETIC .	<b>**</b> 0	FS5.4 FS0.4
ADU	FUF STA	LUA	STA	MUF	STA	SLJ	FINI	LDA	STA	ALS	STA	I SK SLJ	SLJ	SLJ	L DA	STA	RUF	ADD	STA	ISK	SLJ	SLJ	LDA
							VGFOS	L00011				+		KINETIC	L00P12					+		KAT2	L00P13
20 7 31434	26 J 91455 20 J 91455	12 2 14302	20 0 01456 12 0 01435	26 2 63341 26 0 01456	27 0 91455	75 0 01212	75 2 000000 5 05	5 4 0 5 0 0	20 0 01455 12 4 04441	05 0 00003 14 0 01455	20 4 04441 50 0 00000	54 4 07600	75 0 01227 50 0 00000	75 y 00000 50 4 00000	12 4 24141	20 3 01455	26 4 04441	14 0 01455	20 4 04441	54 4 07600 75 0 61237	75 5 91236 50 0 00000	75 9 99000 50 4 09000	12 4 53501

FS0,4	76038,4 LUOP13	KAT2	COUNT	COUNT	PM LAYER2 A NAMEIA	NAME1 NAME2A	NAME2 NAME3A	NAMES NAMESA	NAME4 LEVEL2	111LE+3 11TLE1+3	T1 TLE2+3	T1TLE7+3 A2	A1 82	81 C2	تمن	01 E2	E1 TAPUNIT	H16H0 H16HT	START	777778	17B	**************************************	FS1 FS6
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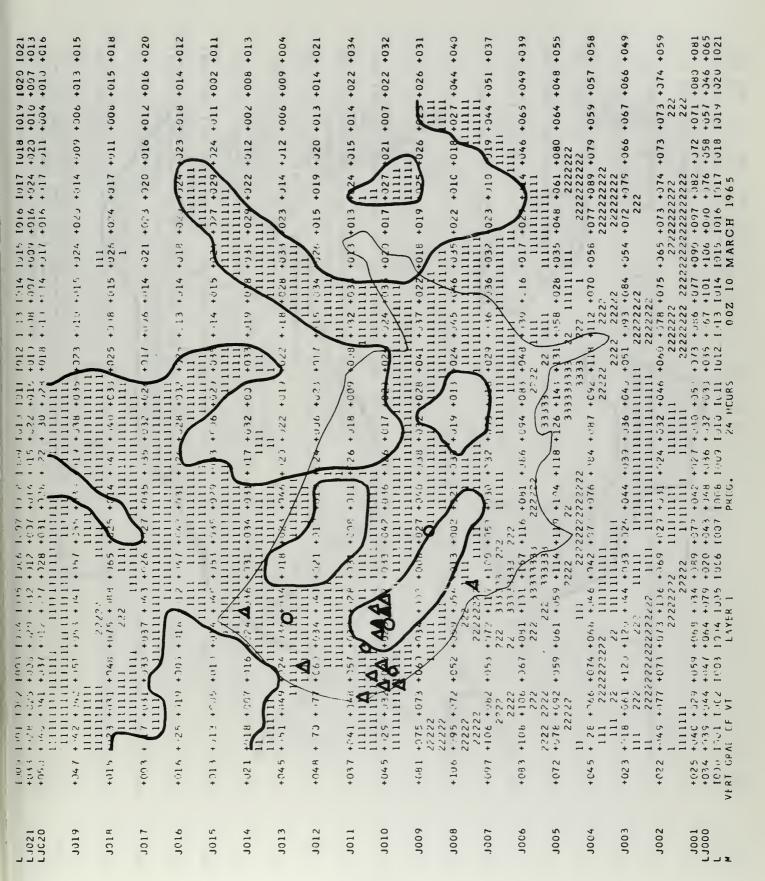
## 10. APPENDIX E

PRINTED FIELDS FROM THE CLEAR AIR TURBULENCE FORECAST

COMPUTER PROGRAM FOR OOZ 10 MARCH 65 THROUGH 12Z 13 MARCH 65

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1020 +440 +415	+38	+31	+27	+301	+332	+361	+41	+485	+552	+584		009 <b>+</b>	+634	+685	174		+788	+820	+84(	+843	+837 +843 1020
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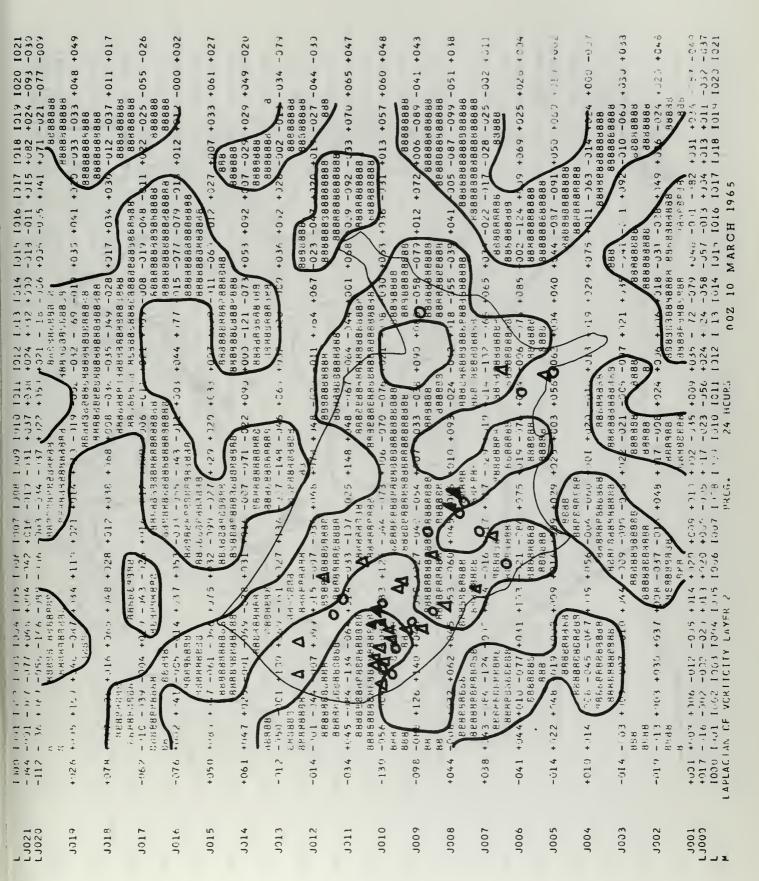
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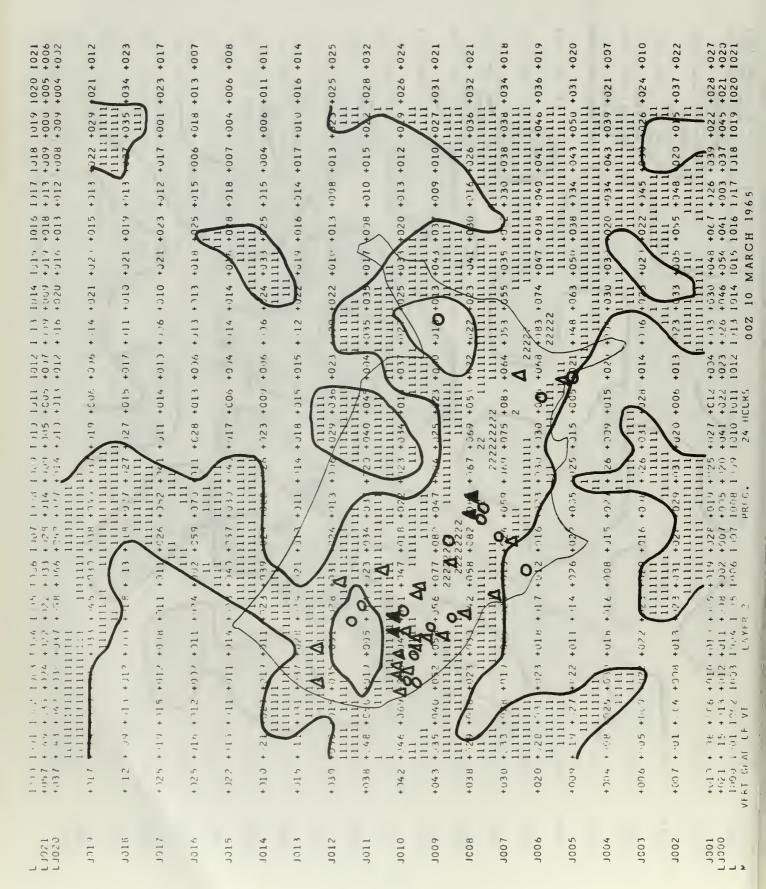


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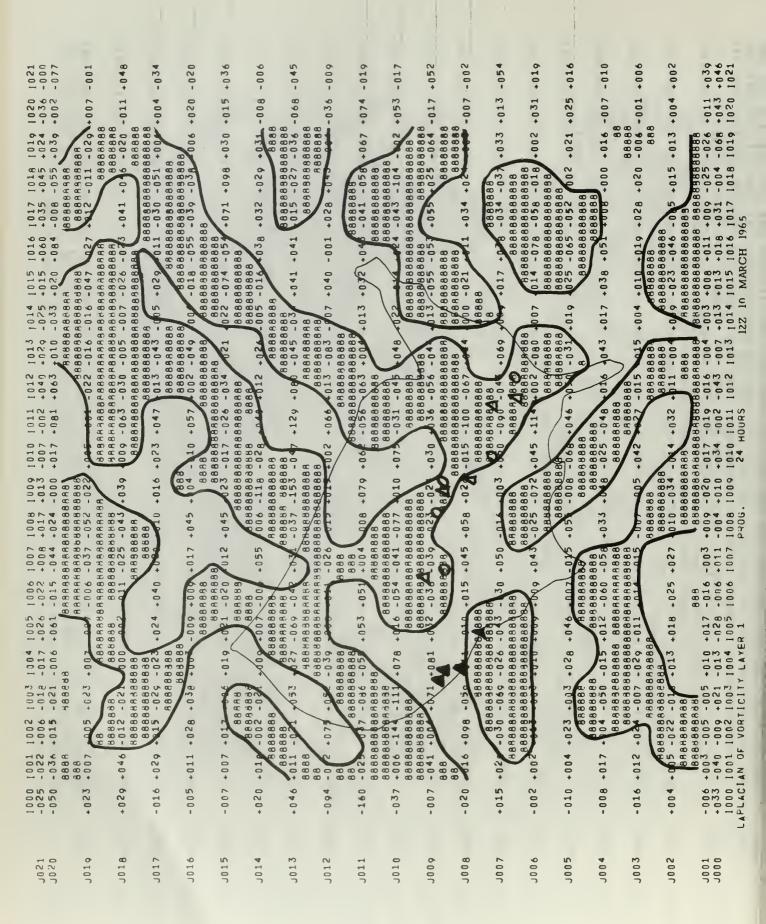


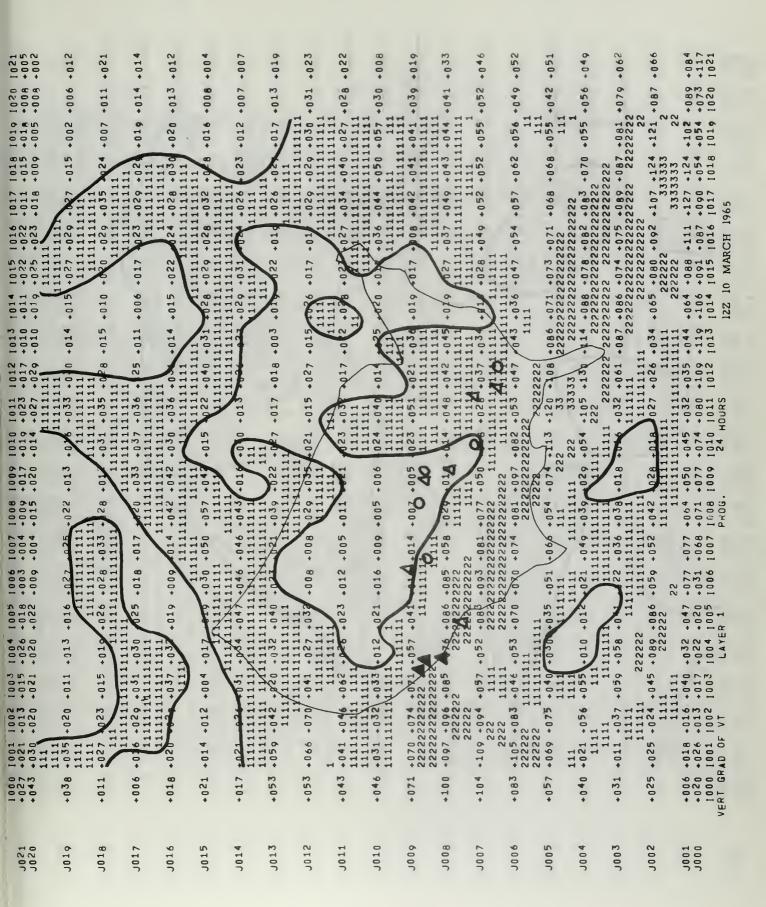


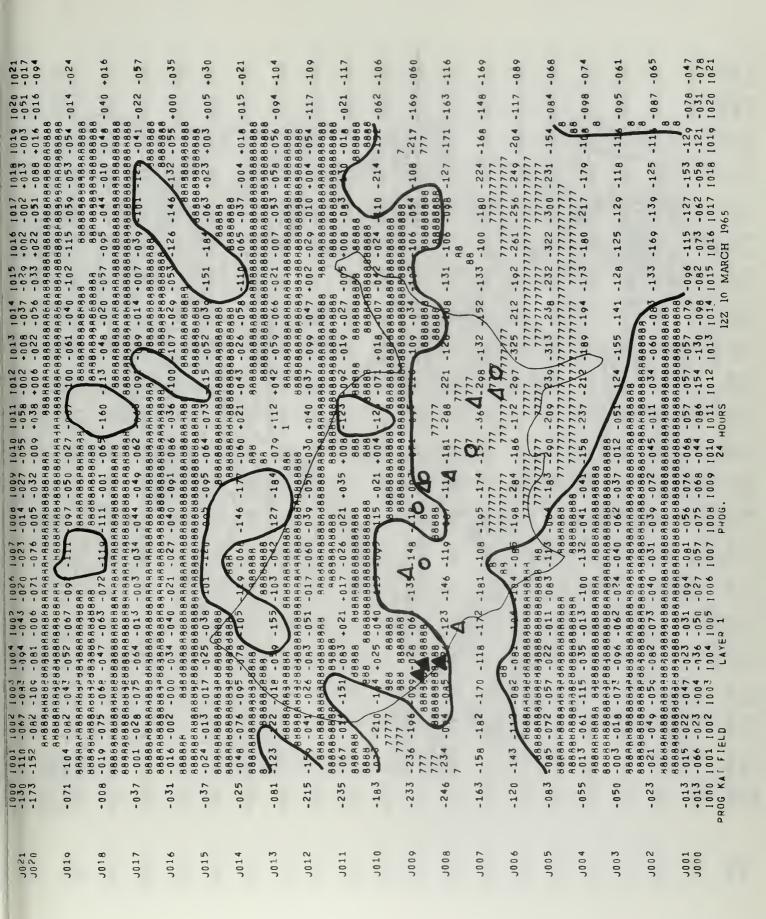
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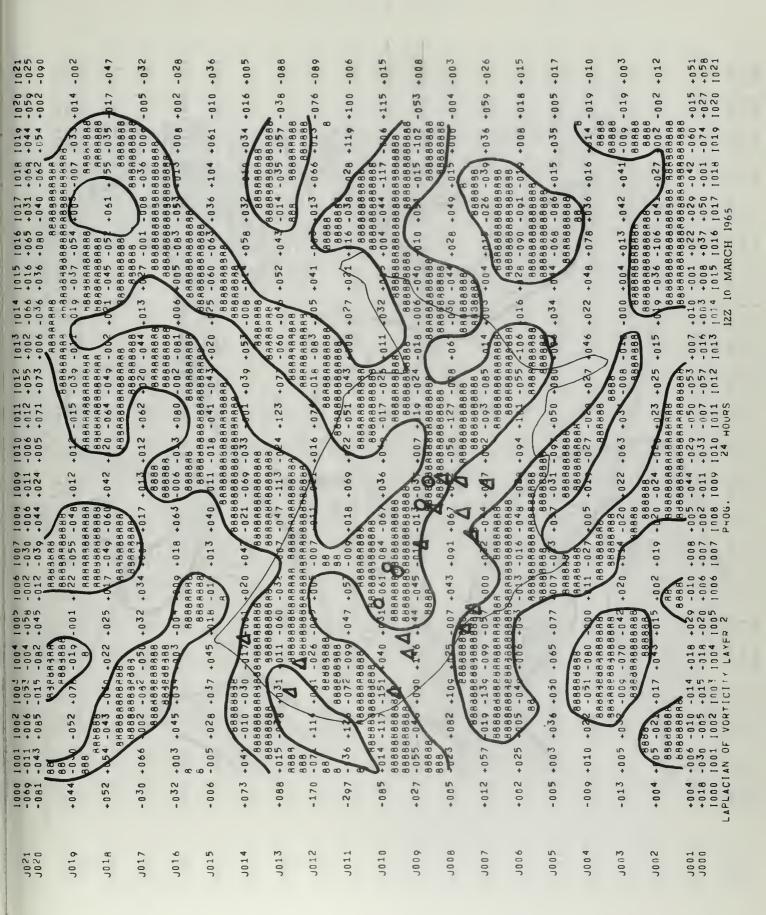
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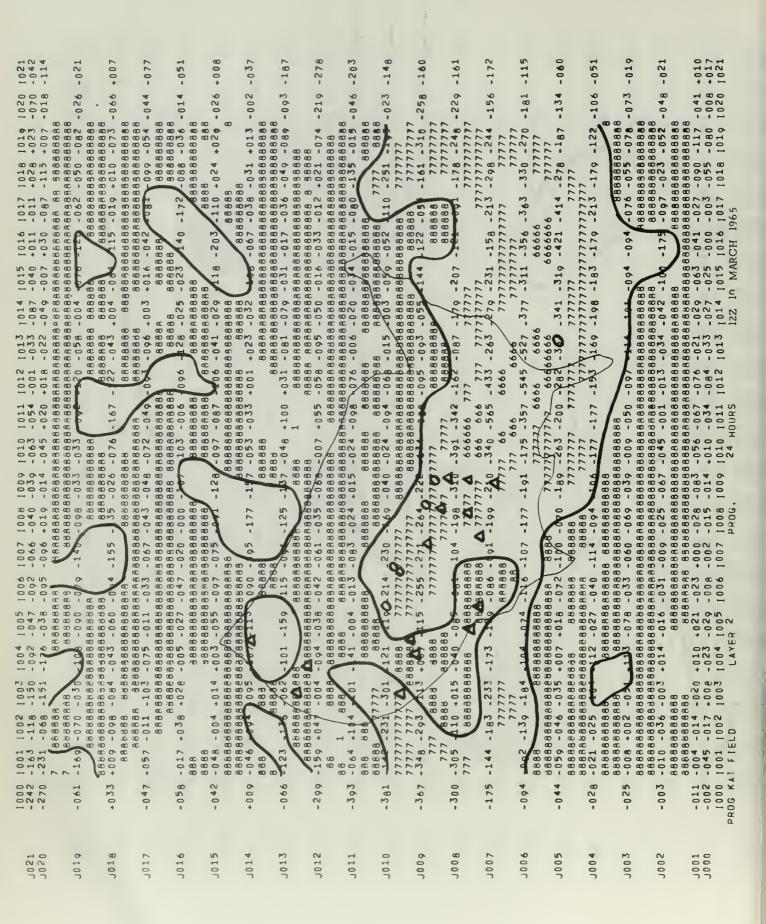


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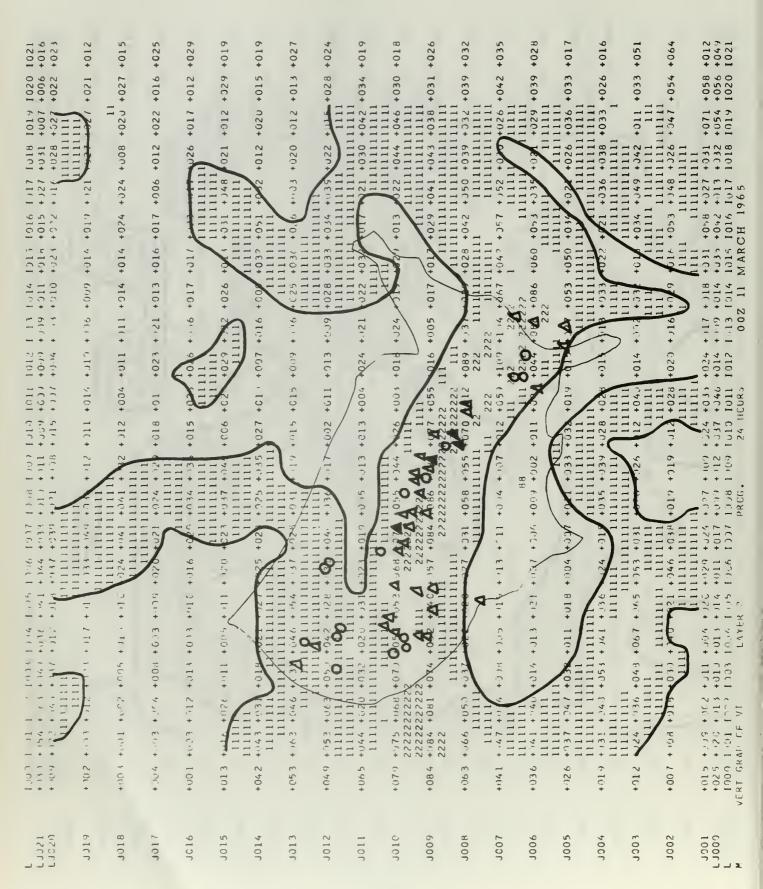
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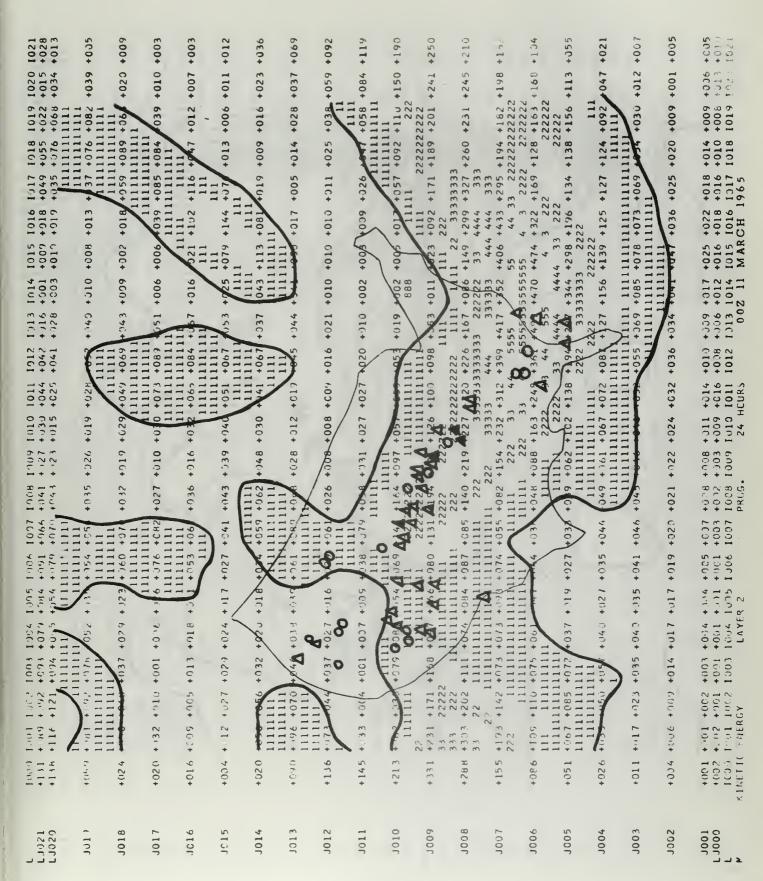
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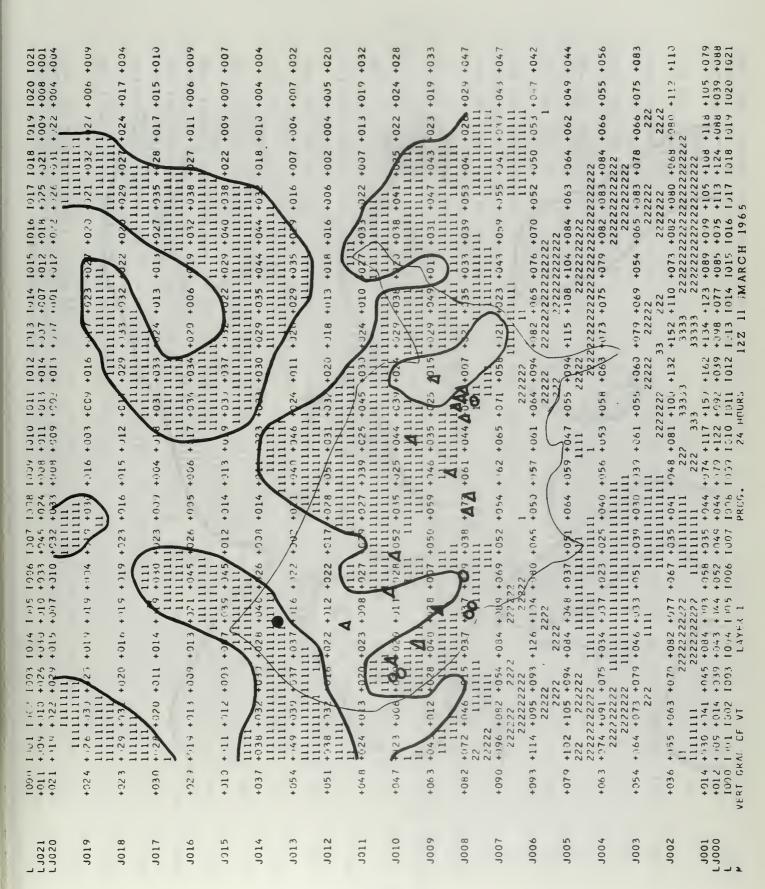


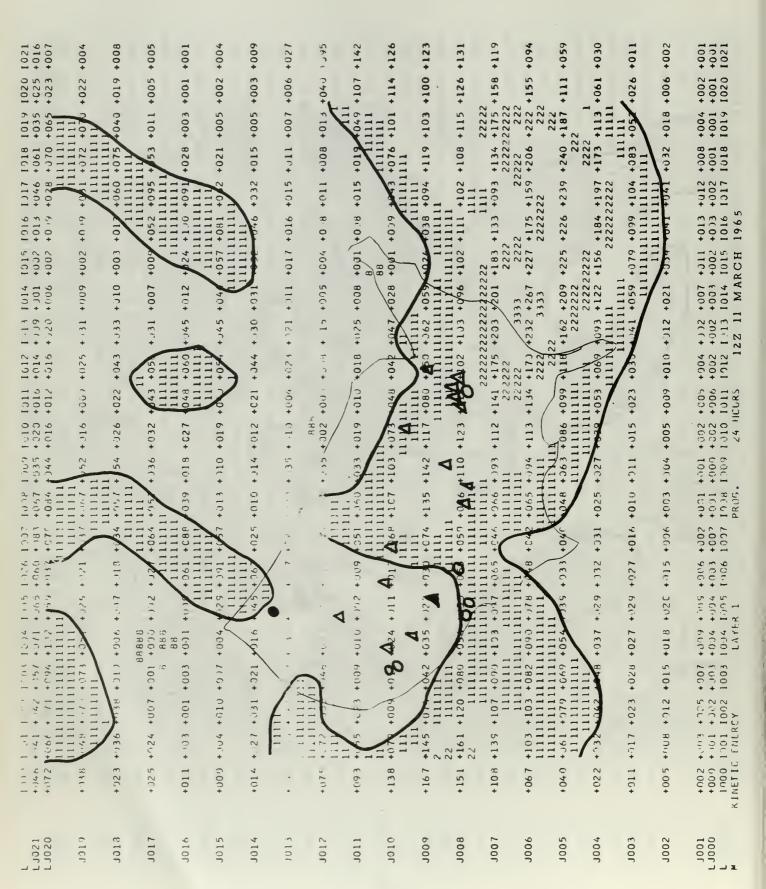


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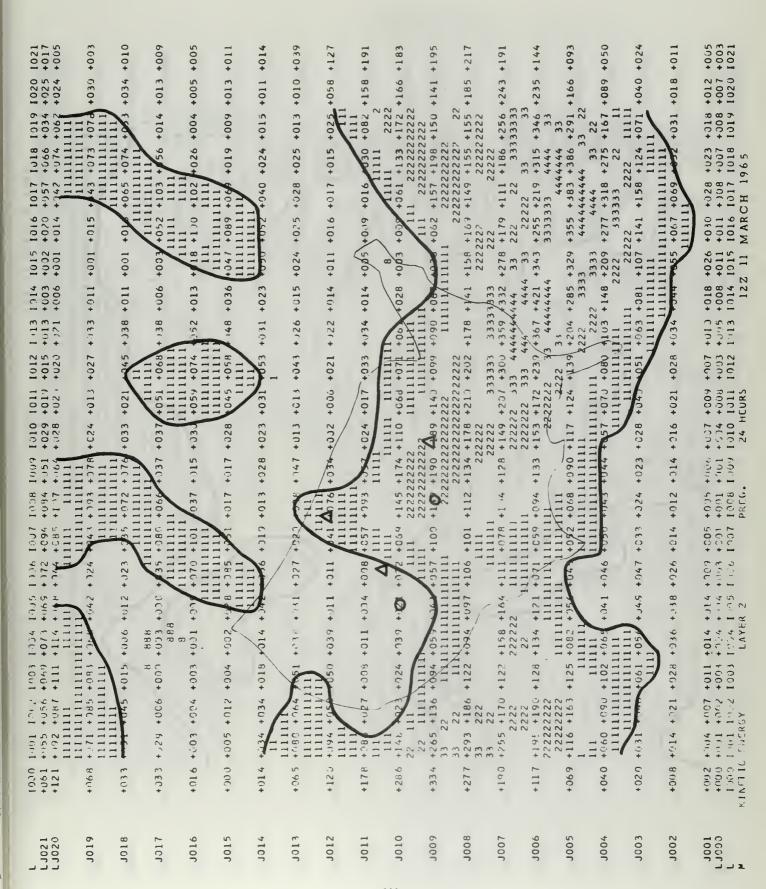




1336   1507   1508   1309   1510   1511   1512   1513   1514   1515   1516   1517   1518   15   -0.56   -1.38   -1.49   -0.54   -0.33   -0.32   -0.13   -0.21   +0.08   -0.37   -1.24   -0.70   -0.   -0.17   -0.74   -1.31   -0.65   -0.02   +0.01   -0.11   -0.15   -0.46   -0.19   +0.11   -0.99   -1.68   -0.8888   888888   8868888888   88688888   8868888   8868888   8868888   8868888   8868888   88688888   88688888   88688888   88688888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   88688888   886888   886888   8868888   8868888   886888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   8868888   886888   8868888   886888   886888   8868888   8868888   8868888   886888   886888   886888   886888   886888   886888   8868888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   886888   88688   886888   8868888   88688   886888   886888   886888   88688   88688   886888   886888	888 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8888 888888888888 88888888888888888888	24 888888888888888888888888888888888888	-019 -092 -028 -010 -122 -112 -017 -022 -085 -087 -065 -102 -153 -100 -036 +005 +001 8888888888888888888888888888888888	0.15 139 -177 -058 +001 -032 -065 -111 - 350 -040 -162 -16 -081 -052 -033 888 888 888 888 888 888 888 888 888	1966-173 144 +018 +011 -037 +004 -078 -199 -025 -044 -093 -065 -032 -019 1888 8888 8888 8888 888	2000 000 000 000 000 000 000 000 000 00	108         -11         -123         -059         +021         -029         -164         102         +006         -010         -058         -014         -012         -012         -072           #888888888888888888888888888888888888	61 - 108 - 023 - 901 - 026 - 185 - 154 - 039 - 083 - 030 - 040 - 039 - 004 - 008 + 006 - 0 88888888888888888888888888888888888	170 - 249	1442 +513 + 122 -054 103 -134 -143 -176 -131 +038 -937 -089 119 -188 -184 -135 -033 8888888888888888888888888888888888	27 (087 - 078 - 258 - 172 - 286 - 043 - 109 - 160 - 136 - 154 - 15	-251 -102 -189 -257 -097 -05 -171 -194 -180 -217 -210 -267 -534 -175 -095 -190 -214 -1	248 -124 -02 -109 -141 -113 -145 -232 -191 -199 -288 -323 -287 -259 -34C -373 77	375 - 080 - 080 - 080 - 083 - 122 - 135 - 127 - 127 - 126 - 324 - 336 - 329 - 341 - 1717 - 17	17 - 0.75 - 0.27 - 0.61 - 0.85 - 0.66 - 0.99 - 1.37 - 11.10 - 1.89 - 2.02 - 2.55 - 2.73 - 1.888 888 88 88 88 88 88 88 88 88 88 88 8	8 -174 -074 -075 -121 -065 -016 -042 -075 -075 -076 -105 -105 -114 -135 -153 -153 -153 -153 -153 -153	1115 1976 - 959 - 634 - 647 - 971 - 382 BBB BBB BBB BBB BBB BBB BBB BBB BBB B	079 - (97 - 061 - 533 - 058 - 375 - 136 - 135 - 163 - 178 - 130 - 077 - 119 - 121 - 598 - 658 -
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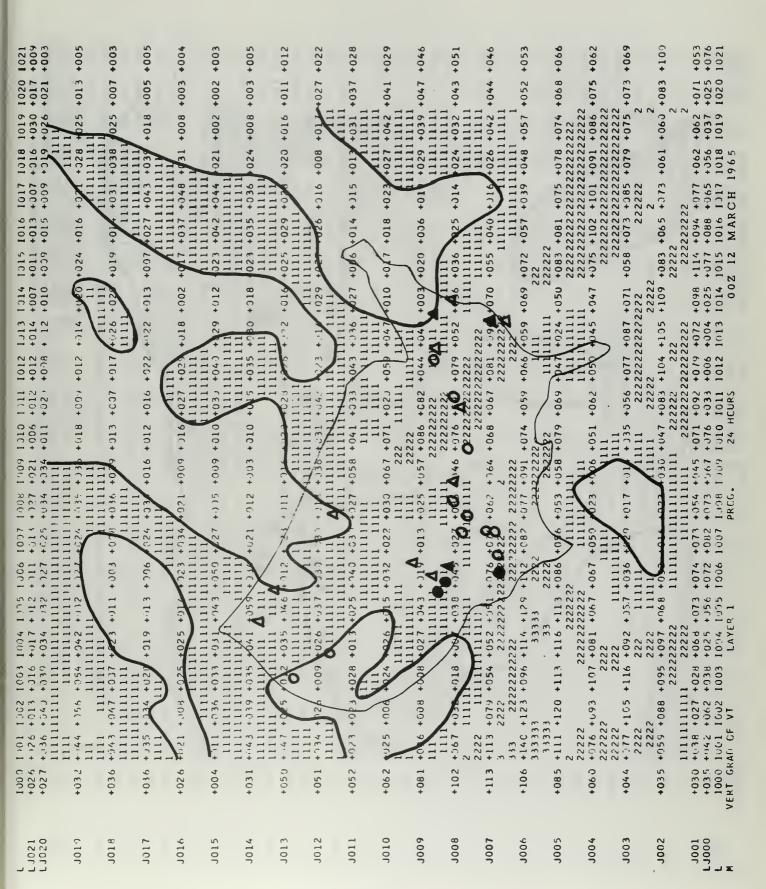
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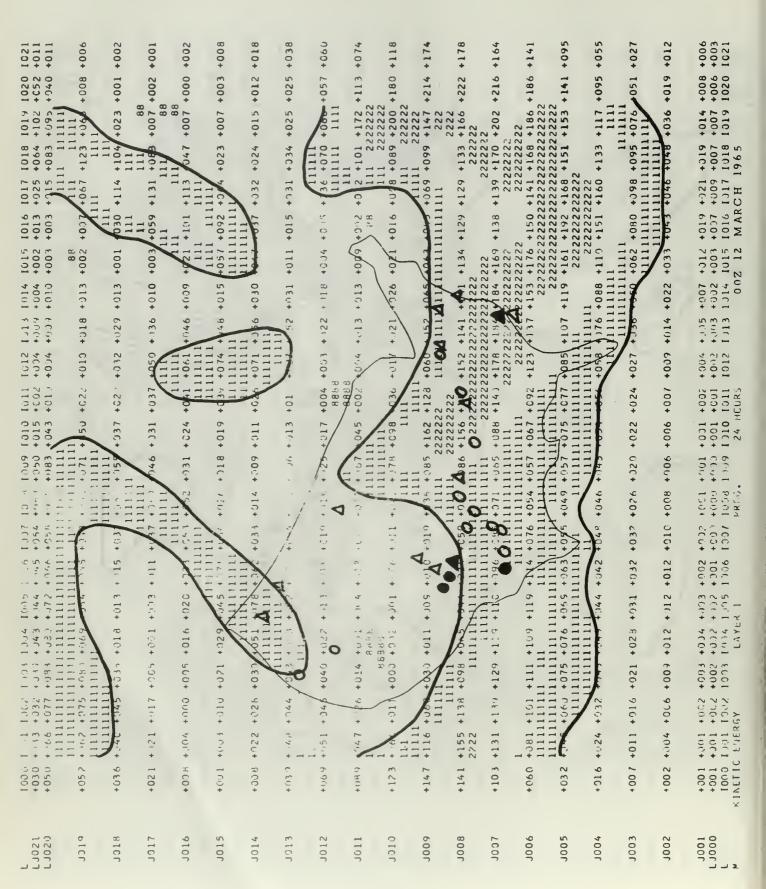


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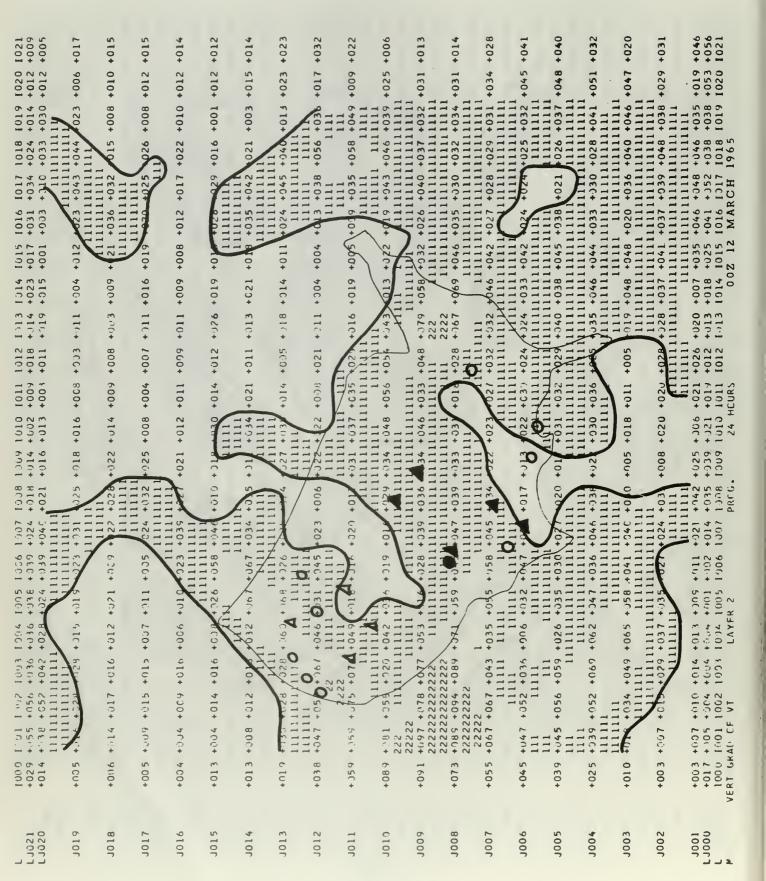




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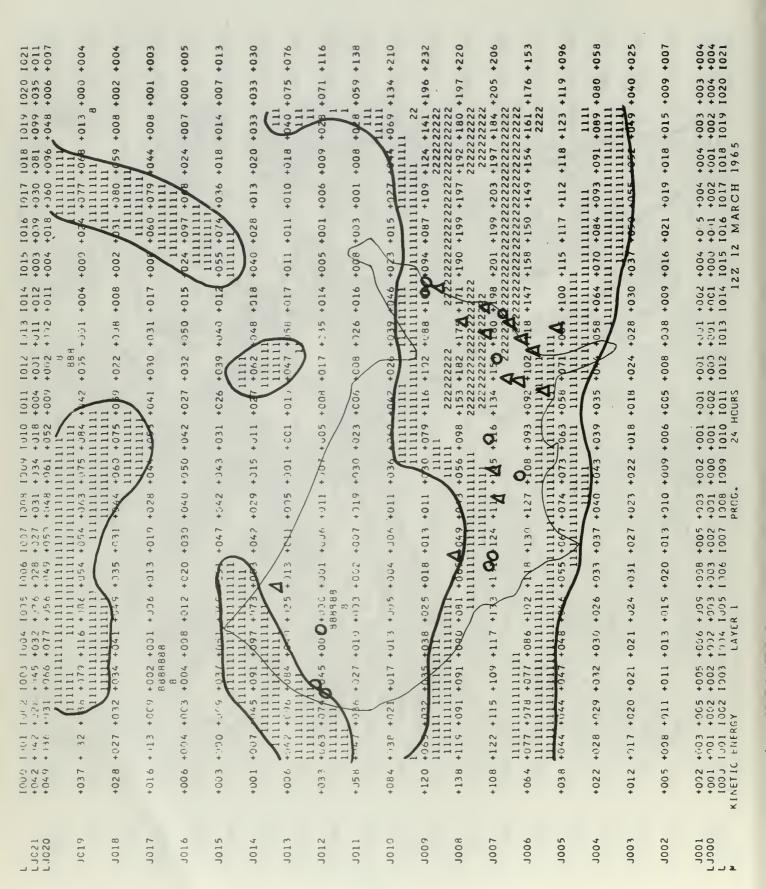
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L 1021 L 1020	91019	1017	J016	3015	J014	5101	3012	1001	0100	9000	9008	1000	9006	3005	700f	1003	1002	J0001 LJ000

## TABLE 1

## AIRCRAFT TURBULENCE CRITERIA

CATEGORY DEFINITION A turbulent condition during which LIGHT occupants may be required to use seat belts, but objects in the aircraft remain at rest. MODERATE A turbulent condition in which occupants require seat belts and occasionally are thrown against the belt. Unsecured objects in aircraft move about. A turbulent condition in which the SEVERE aircraft momentarily may be out of control. Occupants are thrown violently against the belt and back into the seat. Objects not secured in the aircraft are tossed about. EXTREME A rarely encountered turbulent condition in which the aircraft is violently tossed about, and is practically impossible to control. May cause structural damage to the aircraft.

FIELDS	DATE	TIME	LAYER	TOTAL = t	% CORR	L to	M ≠ CORR	M ₹ OCCR (	# CORR	M to	o S ≆ CORR	S =+ 00CR	# CORR
LAPLACIAN OF VORTICITY	10 MAR 65	002	I	19	79	11	7	9	5	2		0	0
VERTICAL GRADIENT OF THERMAL WIND	11	=	11	=	63	11	00	9	7	2	0	0	0
KINETIC ENERGY	-	1	11	:	26	11	3	9	2	2	O	0	0
KAT FIELD	11	=	-	1	3.2	=	5	9		C1	×	~	0
LAPLACIAN OF VORTICITY	10 MAR 65	=	ΙΙ	42	67	22	16	16	<sub>∞</sub>	<b>\</b> †	\d	0	0
VERTICAL GRACIENT OF THERMAL WIND	11	11	11	11	90	22	22	16	12	7	\1	0	0
KINETIC ENERGY	11	Ξ	11	11	86	22	19	16	13	7	à	ŋ	ن
KAT FIELD	п	=	1	12	92	22	17	16	12	7	3	0	0
LAPLACIAN OF VORTICITY	10 MAR 65	122	I	14	71	9	5	5	5	3	C	0	0
VERTICAL GRADIENT OF THERMAL WIND	=	Ξ	:	12	57	9	3	5	2	3	3	0	0
KINETIC ENERGY	Ξ	=	п	11	93	9	9	5	5	3	2	0	0
KAT FIELD	=	=	11	2	71	9	9	5	7	3	0	0	0
LAPLACIAN OF VORTICITY	10 MAR 65	11	II	21	7.1	15	6	9	9	0	0	0	0
VERTICAL GRADIENT OF THERMAL WIND	11	11	11	н	90	15	13	6	9	0	0	0	0
KINETIC ENERGY	п	:	1	п	06	15	13	6	9	0	0	0	0
KAT FIELD	Ξ	ā	Ξ	Ξ	90	15	13	t)	Ω	(	0	0	0

TABLE 3

				TOTAL #	2/2	L to	M	~	M	M	to S		S
FIELDS	DATE	TIME	LAYER	OF OCCR	CORR	₹ OCCR	# CORR	≠ OCCR	÷ CORR	÷ OCCR	=F CORR	# OCCR	=+ CORR
LAPLACIAN OF VORTICITY	12 MAR 65	200	I	27	52	11	7	11	9	2	1	3	1
VERTICAL GRADIENT OF THERMAL WIND	=	Ξ	=	=	92	11	10	11	10	2	2	3	3
KINETIC ENERGY	11	1		Ξ	70	11	9	11	10	2	1	3	1
KAT FIELD	11	-		11	59	11	7	11	7	2	-	~	1
LAPLACIAN OF VORTICITY	12 MAR 65	200	II	19	53	7	2	6	5	5	2	1	1
VERTICAL GRADIENT OF THERMAL WIND	Ξ	=	=		89	7	3	6	8	2	5	1	1
KINETIC ENERGY	Ξ	11	Ξ	п	63	4	1	6	2	2	2	1	7
KAT FIELD	11	н	11	11	48	4	2	6	5	5	2	1	1
LAPLACIAN OF VORTICITY	12 MAR 65	122	T	26	77	15	10	11	8	0	0	0	0
VERTICAL GRADIENT OF THERMAL WIND	1	=	=		100	15	15	11	11	0	0	0	0
KINETIC ENERGY	Ξ	Ξ	=		88	15	13	11	10	0	0	0	0
KAT FIELD	1	=	Ξ	Ξ	92	15	14	11	10	0	0	0	0
LAPLACIAN OF VORTICITY	12 MAR 65	122	II	16	81	12	6	2	2	2	2	0	0
VERTICAL GRADIENT OF THERMAL WIND	11	- 11	1	=	94	12	11	2	2	2	2	0	0
KINETIC ENERGY	-	=	Ξ	=	76	12	11	2	2	2	2	0	0
KAT FIELD	=	Ξ	11	Ξ	87	12	11	2		2	2	0	0

	N.			4		111								
SEVERE	9				67	100	33	50						
MODERATE TO SEVERE	28				71	93	78	09						
MODERATE	103				71	89	76	70						
LIGHT TO MODERATE	165				65	06	70	7.2						
All Categories	302										89	90	76	7.0
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13. ABSTRACT

There is much disagreement as to (a) what causes clear air turbulence (turbulence which is not in or near convective clouds and is above 15,000 feet in altitude) and (b) which meteorological parameters can be used to detect and forecast its occurrence. The approach to this problem has been to relate not one parameter to clear air turbulence but various parameters. By summing these parameters areas can be defined where there is a high probability of encountering clear air turbulence. Each parameter has been based on a statistical study which found a relationship with clear air turbulence. The parameters used were horizontal and vertical shear, curvature, kinetic energy and their derivatives. The numerical forecasting program proposed here can be extended to the stratosphere when more reliable height and temperature fields are available. This program will have much more significance when intermediate forecast height fields, temperature fields and a grid of much smaller mesh length are available.

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